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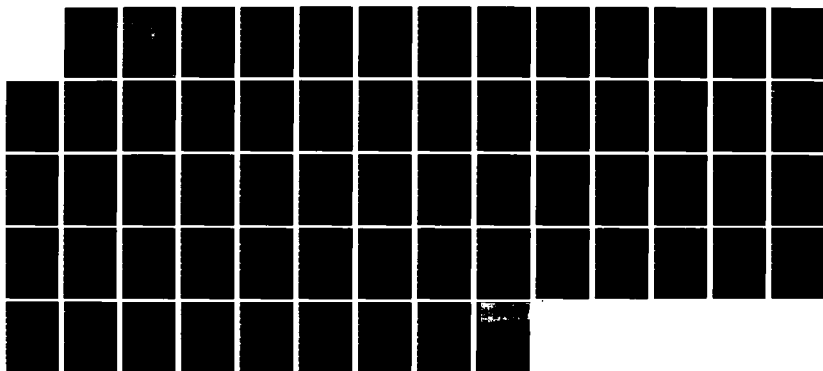
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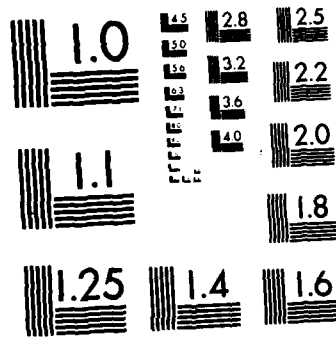
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NAVAL POSTGRADUATE SCHOOL  
Monterey, California



THESIS



A LINEAR APPROXIMATION OF THE SOURCE  
POSITION USING MULTIPLE MAD

by

Wolf-Hubertus Bock

September 1983

Thesis Advisor: Andrew R. Ochadlick, jr.

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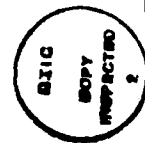
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achieved when the platform is on cardinal headings, and when the target moment has a strong vertical component.



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**A Linear Approximation of the Source  
Position Using Multiple MAD**

by

Wolf-Hubertus Bock  
Lieutenant, United States Navy  
B.A., Rice University, 1975

Submitted in partial fulfillment of the  
requirements for the degree of

**MASTER OF SCIENCE IN SYSTEMS TECHNOLOGY  
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from the

NAVAL POSTGRADUATE SCHOOL  
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## ABSTRACT

For certain assumptions, an analysis of multiple MAD signals results in a reasonable estimate for the localization of a target relative to the MAD platform. This is achieved by using selective approximations to linearize an initially nonlinear problem. The simulation ignores noise and requires an estimate of the magnitude of the target magnetic moment components. Results indicate that the best localization estimates are achieved when the platform is on cardinal headings, and when the target moment has a strong vertical component.

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# TABLE OF SYMBOLS

$\vec{b}_d$	magnetic field vector of the target dipole
$\vec{B}_e$	earth's magnetic field vector
$\vec{B}_t$	total magnetic field vector
$\hat{e}$	earth's magnetic field unit vector
$e_x, e_y, e_z$	components of $\hat{e}$ in cartesian coordinates
$\vec{r}$	vector from the target to the platform
$r$	scalar magnitude of $\vec{r}$

## I. INTRODUCTION

### A. BACKGROUND

Ever since the operational introduction of the MAD (Magnetic Anomaly Detection) system in 1944, it has been a single sensor system limited to indicating detection only. The short ranges of the early versions allowed a general localization if a signal was detected. The use of multiple sensors should allow for a good estimate of the target's location relative to the sensor platform, assuming that the arrangement of the sensors is such that the received signals are linearly independent of one another. Previous attempts to solve this problem have in general focused on the use of only two sensors, but did not develop a usable solution to operational completion. Work has been done on this topic by Wynn et al., [Ref. 1], using a superconducting gradiometer array. The measured signals in their work were subjected to a novel signal processing technique which, in the laboratory, was used to invert the dipole field equation to determine both the position and the moment vectors of a dipole signal source. This thesis approaches the same problem by simulating five standard total field measurements. As shown in Figure 1.1, four magnetometers moving in parallel paths are used to obtain these measurements. The advantage of this approach compared to that of Wynn et al. is that it utilizes existing technology in conjunction with approximations, delineated in Chapter 3, in order to produce a usable result.

## B. APPROACH

The problem of localizing a target from any platform involves at least three unknowns:  $r_x$ ,  $r_y$ , and  $r_z$ , the components of the position vector from the platform to the target. In the case of using MAD, three additional unknowns  $m_x$ ,  $m_y$ , and  $m_z$ , the components of the target's magnetic moment, are also involved. The result is that there are six unknowns that must be solved for in order to localize a target using MAD. Since a normal sized magnetic target can be approximated by the magnetic field of a dipole [Ref. 2], it was decided to use the dipole equation as described in [Ref. 3] to generate the signals used in this simulation. Equation 1.1 describes the MAD signal, and will be developed from the dipole equation in chapter 2. Equation 1.1 is non-

$$S(\vec{r}) = -(m_x + m_y + m_z) / r^3 + 3(m_x r_x + m_y r_y + m_z r_z) (r_x^2 + r_y^2 + r_z^2) / r^5 \quad (\text{eqn 1.1})$$

linear in the unknowns. The position vector in equation 1.1 is defined as going from the target to the platform; this is a consequence of using the dipole equation, and will be explained later.

The cartesian coordinates are defined in Figure 1.2. The z axis is in the direction of platform motion, and the y axis is vertical down. The components of the earth's field unit vector,  $e_x$ ,  $e_y$ , and  $e_z$ , are assumed to be known quantities. Since it is very difficult to explicitly solve a set of non-linear equations in six unknowns, the problem will be simplified by making assumptions and dividing it into two special cases. The first case is a trivial one in which the target's position is assumed known. For this case, equation 1.1 is linear in the three unknowns  $m_x$ ,  $m_y$ , and  $m_z$ . If the three measurements are linearly independent, then Cramer's Rule, [Ref. 4], may be used to solve for these unknowns. The

second case is the more difficult one, and it is the problem investigated in this thesis. In this case, the assumption is made that the target's magnetic moment is known. That reduces equation 1.1 into a non-linear equation in only three unknowns,  $r_x$ ,  $r_y$ , and  $r_z$ . If this simplified version of equation 1.1 could be manipulated into a linear form by using several sensors and appropriate combinations of signals, the position of the target could easily be solved for.

This thesis will develop an approximate solution to this problem by using combinations of the total field signals of an idealized multiple MAD system.

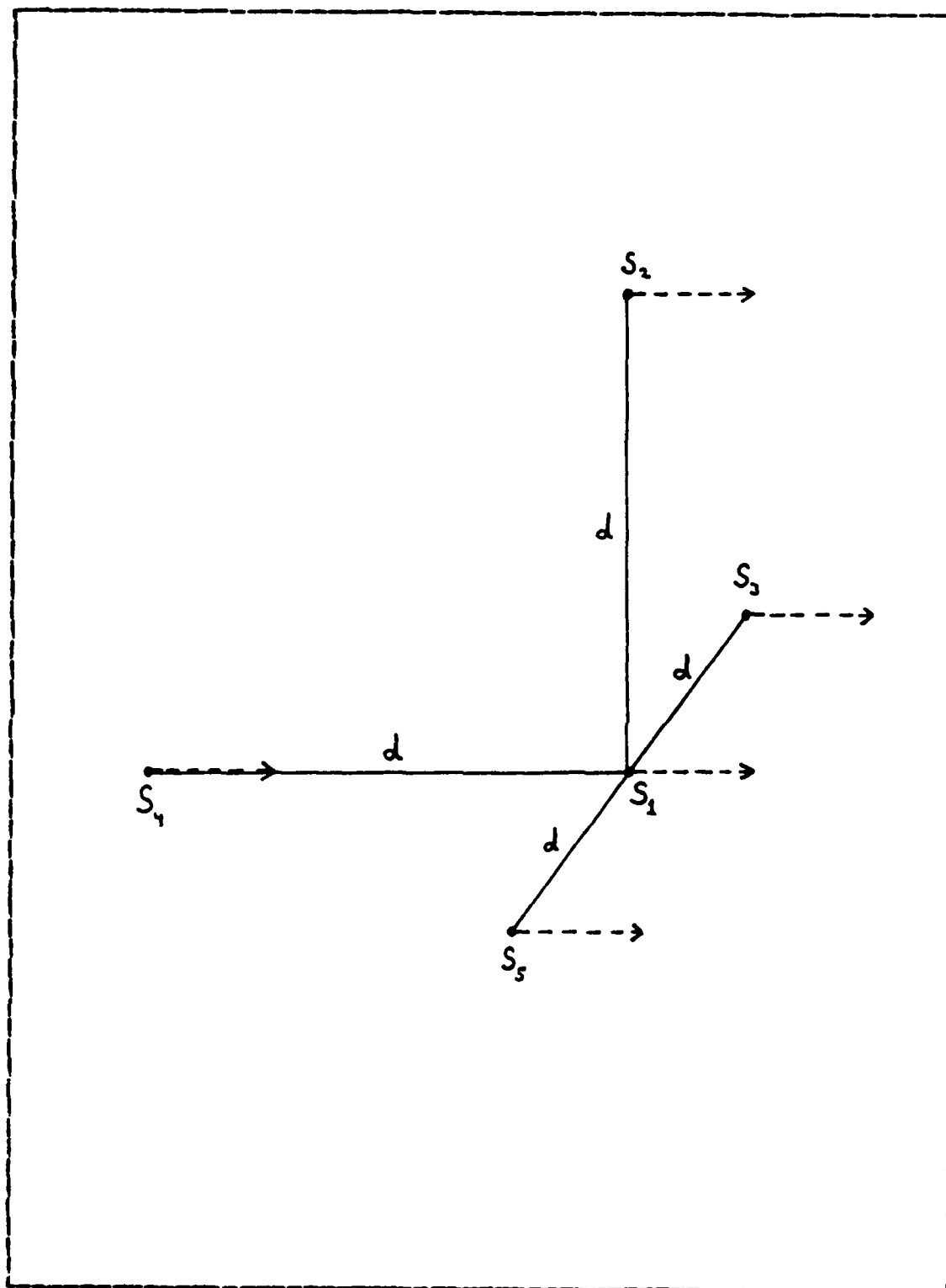


Figure 1.1 Spatial Relationship of Sensor Positions.

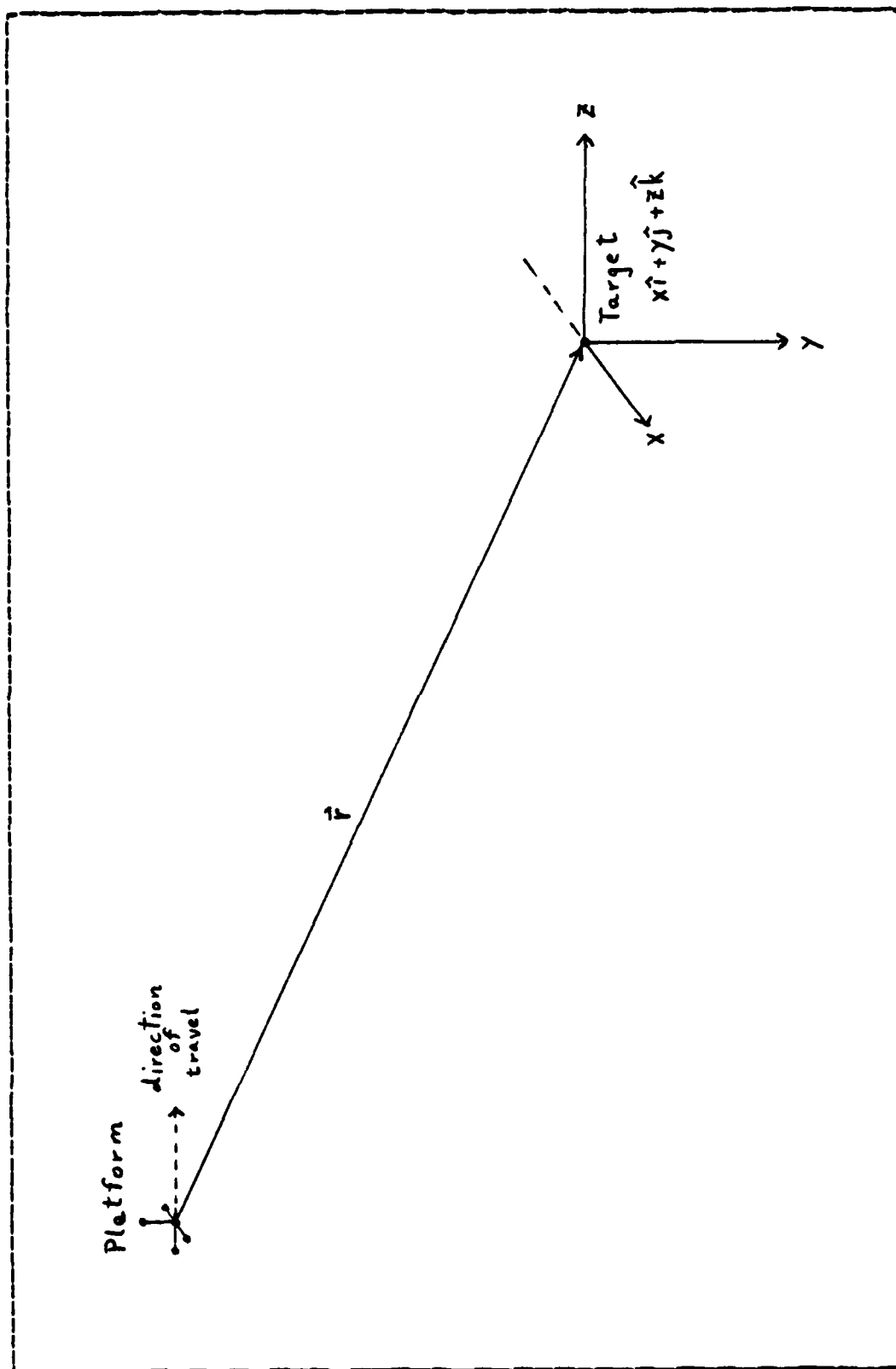


Figure 1.2 Spatial Relationship of Platform and Target.

## II. THEORY

The total field magnetometer measures the magnitude of the vector sum of the ambient magnetic field of the earth and the magnetic field of a magnetic dipole moment. The field of the dipole will be used to represent the magnetic field of the target. The magnitude of the vector sum is called the total field as given by

$$\vec{B}_t = |\vec{B}_e + \vec{b}_d|$$

$\vec{B}_e$  represents the earth's magnetic field vector and  $\vec{b}_d$  represents the field due to a magnetic dipole. In the general case of interest here, the magnitude of the dipole field is much less than the magnitude of the earth's field. Under certain conditions, a useful approximation to the total field may be derived from the geometry shown in Figure 2.1.

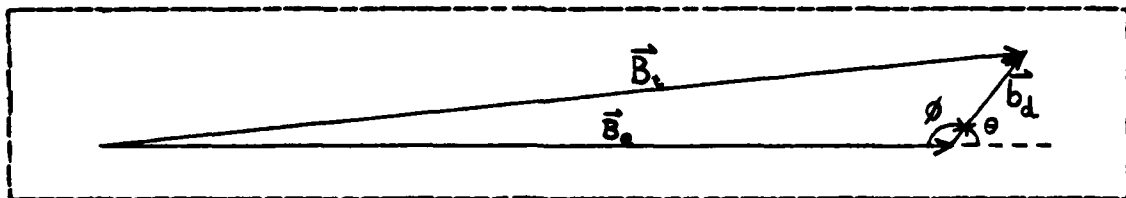


Figure 2.1 Vector Relationship of  $\vec{B}_t$ ,  $\vec{b}_d$ , and  $\vec{B}_e$ .

In this figure a very small vector is added to a very large one. The vectors of Figure 2.1 are not to scale.  $\vec{b}_d$  is to be considered several orders of magnitude smaller than  $\vec{B}_e$ . The application of basic geometric formulas for the sides of a triangle and the angle between sides yields

$$B_t^2 = B_e^2 + b_d^2 - 2b_d B_e \cos \phi$$

for the geometry of Figure 2.1 . In terms of  $\theta$  this equation becomes

$$B_t^2 = B_e^2 + b_d^2 + 2b_d B_e \cos\theta$$

The  $B_e^2$  term can be factored out of the right hand side of the equation to produce

$$B_t^2 = B_e^2 \{1 + (b_d/B_e)^2 + 2(b_d/B_e) \cos\theta\}$$

Taking the square root yields equation 2.1 .

$$B_t = B_e \{[1 + (b_d/B_e)^2 + 2(b_d/B_e) \cos\theta]^{1/2}\} \quad (\text{eqn 2.1})$$

Since by assumption  $b_d$  is much less than  $B_e$ , the term  $(b_d/B_e)^2$  is much less than  $2(b_d/B_e) \cos\theta$  and can be considered negligible. This reduces equation 2.1 to

$$B_t = B_e \{[1 + 2(b_d/B_e) \cos\theta]^{1/2}\} \quad (\text{eqn 2.2})$$

The general expansion formula given by

$$(1+x)^n = 1 + nx + n(n-1)x^2/2! + \text{Higher Order Terms}$$

can be applied to equation 2.1 . For the case here,  $n=1/2$ , and  $x=(b_d/B_e)^2 + 2(b_d/B_e) \cos\theta$ . Substituting these values into the general expansion formula gives equation 2.1 as

$$B_t = B_e \{1 + .5[(b_d/B_e)^2 + 2(b_d/B_e) \cos\theta] - 1/8[(b_d/B_e)^2 + (2b_d/B_e) \cos\theta]^2 + \text{H.O.T.}\}$$

Squaring the appropriate term and multiplying through by the coefficients results in

$$B_t = B_e \{1 + .5[(b_d/B_e)^2] + (b_d/B_e) \cos\theta - 1/8[b_d/B_e]^4 - 4/8[b_d/B_e]^3 \cos\theta - 4/8[b_d/B_e]^2 \cos^2\theta + \text{H.O.T.}\}$$

The cubed and higher order terms will be considered to be negligible. Dropping those terms and rearranging the remaining ones yields the form

$$B_t = B_e \{ 1 + (b_d/B_e) \cos \theta - .5 (b_d/B_e)^2 \cos^2 \theta + .5 (b_d/B_e)^2 \}$$

Using the relation  $\sin^2 \theta + \cos^2 \theta = 1$ , this reduces to

$$B_t = B_e \{ 1 + (b_d/B_e) \cos \theta + .5 (b_d/B_e)^2 \sin^2 \theta \}$$

After multiplying through by  $B_e$ , the second term can be written in terms of the dot product  $\vec{b}_d \cdot \vec{B}_e / B_e$ . This is reduced to  $\vec{b}_d \cdot \hat{e}$  if the unit vector  $\hat{e}$  is defined as  $\vec{B}_e / B_e$ , and the resulting equation is

$$B_t = B_e + \vec{b}_d \cdot \hat{e} + .5 (b_d/B_e)^2 \sin^2 \theta$$

Since  $b_d$  is on the order of 1nT while  $B_e$  is on the order of 50,000 nT, the error term involving the sine is negligible. For the stated assumptions, equation 2.1 can be represented by

$$B_t = B_e + \vec{b}_d \cdot \hat{e} \quad (\text{eqn 2.3})$$

In this thesis,  $B_e$  will be assumed constant. In addition, this simulation will assume that no noise exists. Thus, the total field magnetometer will measure the anomaly in the earth's field defined by

$$S(\vec{r}) = \vec{b}_d \cdot \hat{e}$$

In this expression,  $\vec{b}_d$  represents the magnetic field of a dipole.  $\vec{b}_d$  is defined [Ref. 3] by the equation

$$\vec{b}_d(\vec{r}) = -\vec{m}/r^3 + 3(\vec{m} \cdot \vec{r})\vec{r}/r^5 \quad (\text{eqn 2.4})$$

$\vec{m}$  is the magnetic dipole moment in units of nTft<sup>3</sup>.  $\vec{r}$  is the position vector to the field point and is measured in feet. If  $b_d$  is much less than  $B_e$ , then equation 2.3 and equation 2.4 result in the equation

$$S(\vec{r}) = -(\vec{m} \cdot \hat{e})/r^3 + 3(\vec{m} \cdot \vec{r})(\vec{r} \cdot \hat{e})/r^5 \quad (\text{eqn 2.5})$$

This equation is an alternative basis for the derivation of the Anderson's Functions, found in [Ref. 5]. The Anderson Functions are a commonly used approximation for the signal received by a MAD sensor. The computer simulation in this thesis is based on equation 2.5 directly, since it is in a representation which is easier to use than the Anderson's function representation of a MAD signal.

### III. NATURE OF THE PROBLEM

This thesis will develop and demonstrate an approximation that generates a reasonable solution of the target's position relative to a platform bearing several "sensors" to "measure" the magnetic signal as the platform makes a straight line encounter near the target. The assumptions are as follows:

- 1.) The dipole equation is a valid representation of the magnetic field of the target.
- 2.)  $b_d$  is several orders of magnitude smaller than  $B_e$ .
- 3.) Measurements are done using only straight line encounters.
- 4.) The target's magnetic dipole moment is a known vector.
- 5.) The earth magnetic field vector is known.
- 6.) The gradient of the earth's field is zero.
- 7.) No magnetic noise of any kind (environment, sensor, etc) exists.
- 8.) The measurements are oriented along four lines which are oriented with respect to the flight path as shown in Figure 1.1.

Since the dipole equation is written with the moment at the origin of a coordinate system, the calculations of the signal field values used in the simulation are made with the target located at the origin. As will be seen, the program performs a coordinate transformation in order to produce the output of target position relative to the platform. After this coordinate transformation, the origin is located at the sensor platform and moves with it.

The five measurements are made along four separate flight paths, so only four different "sensors" are involved.

Sensor 4 could be replaced by inducing a time delay in the measurement of sensor 1. The signals generated at these measurement points are measured at each time step. The position vectors can all be described relative to the origin, located at the target, in terms of the position vector of sensor 1. The measured signals are represented by the following equations:

$$\begin{aligned}
 S(\vec{r}_1) &= -\{(m_x e_x + m_y e_y + m_z e_z)(r_1)^2 - 3(m_x x + m_y y + m_z z)(x e_x + y e_y + z e_z)\} / r_1^5 \\
 S(\vec{r}_2) &= -\{(m_x e_x + m_y e_y + m_z e_z)(r_2)^2 - 3(m_x x + m_y [y-d] + m_z z)(x e_x + [y-d] e_y + z e_z)\} / r_2^5 \\
 S(\vec{r}_3) &= -\{(m_x e_x + m_y e_y + m_z e_z)(r_3)^2 - 3(m_x [x-d] + m_y y + m_z z)([x-d] e_x + y e_y + z e_z)\} / r_3^5 \\
 S(\vec{r}_4) &= -\{(m_x e_x + m_y e_y + m_z e_z)(r_4)^2 - 3(m_x x + m_y y + m_z [z-d])(x e_x + y e_y + [z-d] e_z)\} / r_4^5 \\
 S(\vec{r}_5) &= -\{(m_x e_x + m_y e_y + m_z e_z)(r_5)^2 - 3(m_x [x+d] + m_y y + m_z z)([x+d] e_x + y e_y + z e_z)\} / r_5^5
 \end{aligned}$$

For convenience, the following dummy variables are used in the computer program and are defined as:

$$\begin{aligned}
 G &= m_x e_x + m_y e_y + m_z e_z \\
 V1 &= 3m_x e_x - G \\
 V2 &= 3(m_x e_y + m_y e_x) \\
 V3 &= 3m_y e_y - G \\
 V4 &= 3(m_y e_z + m_z e_y) \\
 V5 &= 3m_z e_z - G \\
 V6 &= 3(m_z e_x - m_x e_z) \\
 S1 &= S(\vec{r}_1) \\
 S2 &= S(\vec{r}_2) \\
 S3 &= S(\vec{r}_3) \\
 S4 &= S(\vec{r}_4) \\
 S5 &= S(\vec{r}_5)
 \end{aligned}$$

The use of these variables reduces the above equations to the following form, which are the defining equations for the signals in the simulation.

$$S1 = (V1x^2 + V2xy + V3y^2 + V4yz + V5z^2 + V6xz) / r_1^5$$

$$\begin{aligned}
S_2 &= (V_1x^2 + V_2xy - V_2xd + V_3y^2 - 2V_3yd + V_3d^2 + V_4yz - V_4dz + V_5z^2 + V_6xz) / r_2^5 \\
S_3 &= (V_1x^2 - 2V_1xd + V_1d^2 + V_2xy - V_2dy + V_3y^2 + V_4yz + V_5z^2 + V_6xz - V_6dz) / r_3^5 \\
S_4 &= (V_1x^2 + V_2xy + V_3y^2 + V_4yz - V_4yd + V_5z^2 - 2V_5zd + V_5d^2 + V_6xz - V_6xd) / r_4^5 \\
S_5 &= (V_1x^2 + 2V_1xd + V_1d^2 + V_2xy + V_2dy + V_3y^2 + V_4yz + V_5z^2 + V_6xz + V_6dz) / r_5^5
\end{aligned}$$

The unknowns of interest are  $x$ ,  $y$ , and  $z$ , which are related to the position vectors as follows:

$$\vec{r}_1 = x\hat{i} + y\hat{j} + z\hat{k} \quad (\text{eqn 3.1})$$

$$\vec{r}_2 = x\hat{i} + (y-d)\hat{j} + z\hat{k} \quad (\text{eqn 3.2})$$

$$\vec{r}_3 = (x-d)\hat{i} + y\hat{j} + z\hat{k} \quad (\text{eqn 3.3})$$

$$\vec{r}_4 = x\hat{i} + y\hat{j} + (z-d)\hat{k} \quad (\text{eqn 3.4})$$

$$\vec{r}_5 = (x+d)\hat{i} + y\hat{j} + z\hat{k} \quad (\text{eqn 3.5})$$

To linearize the problem it will be assumed that the denominators of the equations for  $S_1$ ,  $S_2$ ,  $S_3$ ,  $S_4$ , and  $S_5$  given above are all equal to  $r$ , i.e.,

$$r = r_1 = r_2 = r_3 = r_4 = r_5$$

The equations for  $S_1$ ,  $S_2$ ,  $S_3$ ,  $S_4$ , and  $S_5$  with the denominators equal can then be subtracted from one another to yield the following:

$$S_2 - S_3 = \{(V_2 - 2V_1)x + (2V_3 - V_2)y + (V_4 - V_6)z + (V_1 - V_3)d\} (-d/r^5)$$

$$S_2 - S_5 = \{(V_2 + 2V_1)x + (2V_3 + V_2)y + (V_4 + V_5)z + (V_1 - V_3)d\} (-d/r^5)$$

$$S_3 - S_1 = \{2V_1x + V_2y + V_6z - V_1d\} (-d/r^5)$$

$$S_5 - S_1 = \{-2V_1x - V_2y - V_6z - V_1d\} (-d/r^5)$$

$$S_3 - S_4 = \{(2V_1 - V_6)x + (V_2 - V_4)y + (V_6 - 2V_5)z + (V_5 - V_1)d\} (-d/r^5)$$

$$S_5 - S_4 = \{-(2V_1 + V_6)x - (V_2 + V_4)y - (V_6 + 2V_5)z + (V_5 - V_1)d\} (-d/r^5)$$

Since the denominators are assumed to be identical, if these six equations are divided in pairs the coefficients involving the non-linear  $r^5$  term and the quantity  $d$  are canceled out. This results in the following equations that define the new variables  $A_1$ ,  $A_2$ , and  $A_3$  as

$$A_1 = (S_2 - S_3) / (S_2 - S_5) \quad (\text{eqn 3.6})$$

$$A_2 = (S_3 - S_1) / (S_5 - S_1) \quad (\text{eqn 3.7})$$

$$A_3 = (S_3 - S_4) / (S_5 - S_4) \quad (\text{eqn 3.8})$$

Defining the following variables for convenience,

$$\begin{aligned} C1 &= A1(V2+2V1) - (V2-2V1) \\ C2 &= A1(2V3+V2) - (2V3-V2) \\ C3 &= A1(V4+V6) - (V4-V6) \\ K1 &= [(V1-V3) - A1(V1-V3)]d \\ C4 &= A2(2V1) + 2V1 \\ C5 &= A2(V2) + V2 \\ C6 &= A2(V6) + V6 \\ K2 &= [V1 - A2(V1)]d \\ C7 &= A3(V6+2V1) - (V6-2V1) \\ C8 &= A3(V4+V2) - (V4-V2) \\ C9 &= A3(2V5+V6) - (2V5-V6) \\ K3 &= [(V1-V5) - A3(V1-V5)]d \end{aligned}$$

equations 3.6 - 3.8 can be written in the following form as

$$C1x + C2y + C3z = K1 \quad (\text{eqn 3.9})$$

$$C4x + C5y + C6z = K2 \quad (\text{eqn 3.10})$$

$$C7x + C8y + C9z = K3 \quad (\text{eqn 3.11})$$

These three equations are linear in terms of  $x$ ,  $y$ , and  $z$ . In addition, they are linearly independent as shown by using the program in Appendix B. A sample output demonstrating the linear independence is shown in Appendix C. Since they are linearly independent, Cramer's Rule can be used to solve equations 3.9 - 3.11 for  $x$ ,  $y$ , and  $z$ . The computer program in Appendix A was written in terms of these equations. The program assumes that the magnitude of the target's magnetic moment is  $5 \times 10^8$  nTft<sup>3</sup>. A representative moment was selected by using the values listed by Fromm in [Ref. 2], who lists a moment of  $10^8$  to  $2 \times 10^8$  cgs units for a submarine. One cgs unit is approximately 3.35 nTft<sup>3</sup>. The value used in the program is a rounded out average of Fromm's values. Computations are done using the standard convention with the target dipole at the origin. However, as indicated earlier,

the output is corrected by a coordinate transformation so that the platform is at the origin, and the target position is given with respect to the platform.

#### IV. DISCUSSION

##### A. GENERAL

The program in Appendix B was written to check whether the results generated by the approximation equations were reasonably close to the actual coordinates of the target. The program was modified into the form shown in Appendix A to graphically provide a comparison between the calculated and the actual position coordinates. Initial parameters for the knowns in the equations were a platform heading of  $30^\circ$  magnetic, an earth field vector of  $70^\circ$  down from the horizontal, and a target dipole moment vector with a vertical component  $50^\circ$  down from the horizontal and a horizontal component oriented  $355^\circ$  from magnetic north. These initial parameters have no special significance, and merely represent a convenient starting point. As discussed earlier, the magnitude of the target dipole moment was set at the value of  $5 \times 10^8 \text{ nTft}^3$ . The spacing between measurement positions,  $d$ , was taken as 50 feet, and the platform passed directly overhead the target at 1000 feet. This and all subsequent runs were started at 5000 feet prior to CPA (closest point of approach) with the platform advancing 50 feet per time step. One position calculation was completed at each time step, the simulation ceasing when the platform was 5000 feet past CPA. For interpretation purposes, calculated target positions are shown as the sensor platform moves 10,000 feet past the target in a straight line encounter, with CPA occurring at the 5000 foot point. Neither the CPA nor the target's location are in any way considered known in the localization process. However, as the area of interest is the behavior of the simulation close to CPA, the closest

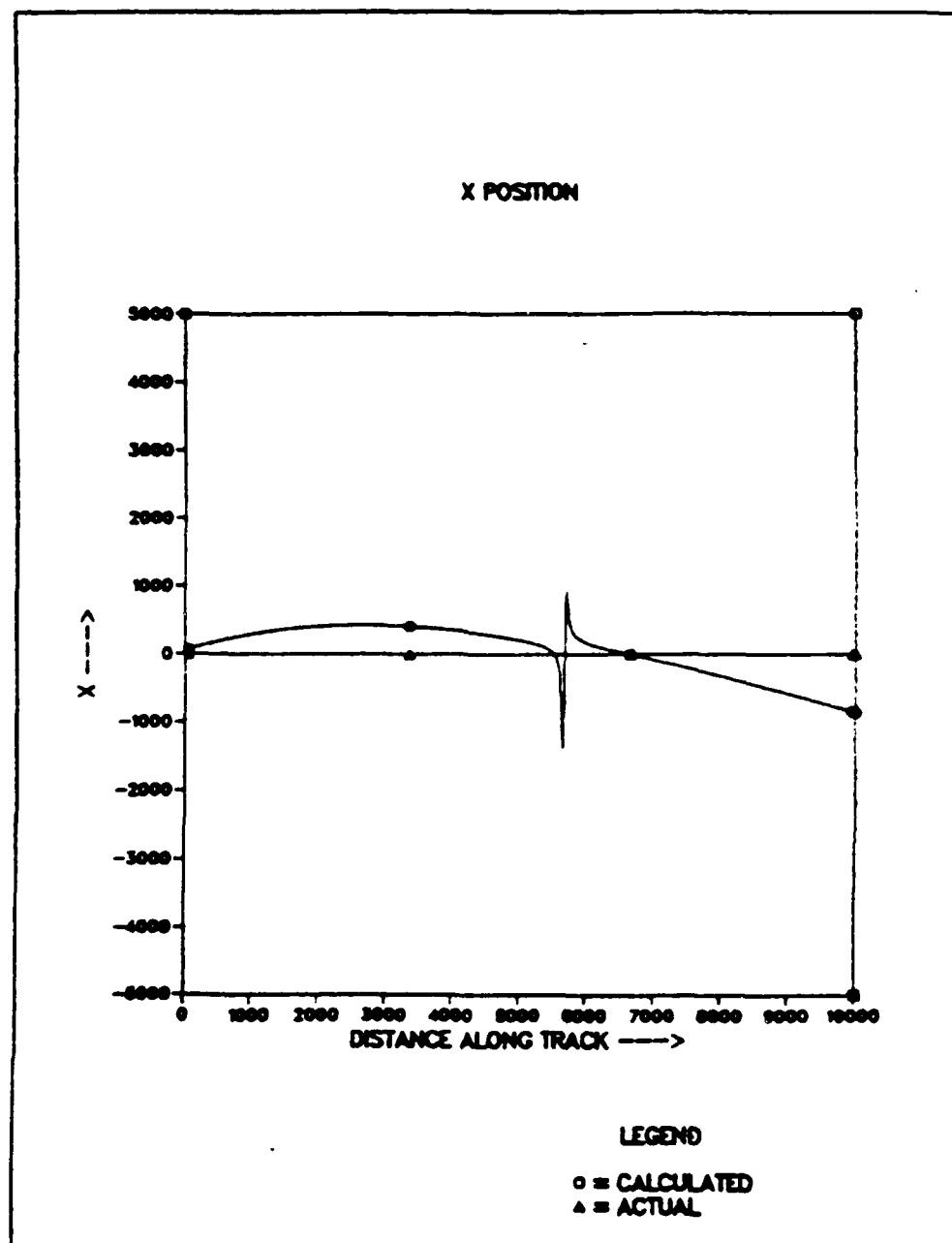


Figure 4.1 Initial Run, x position.

point of approach is always centered in the following figures.

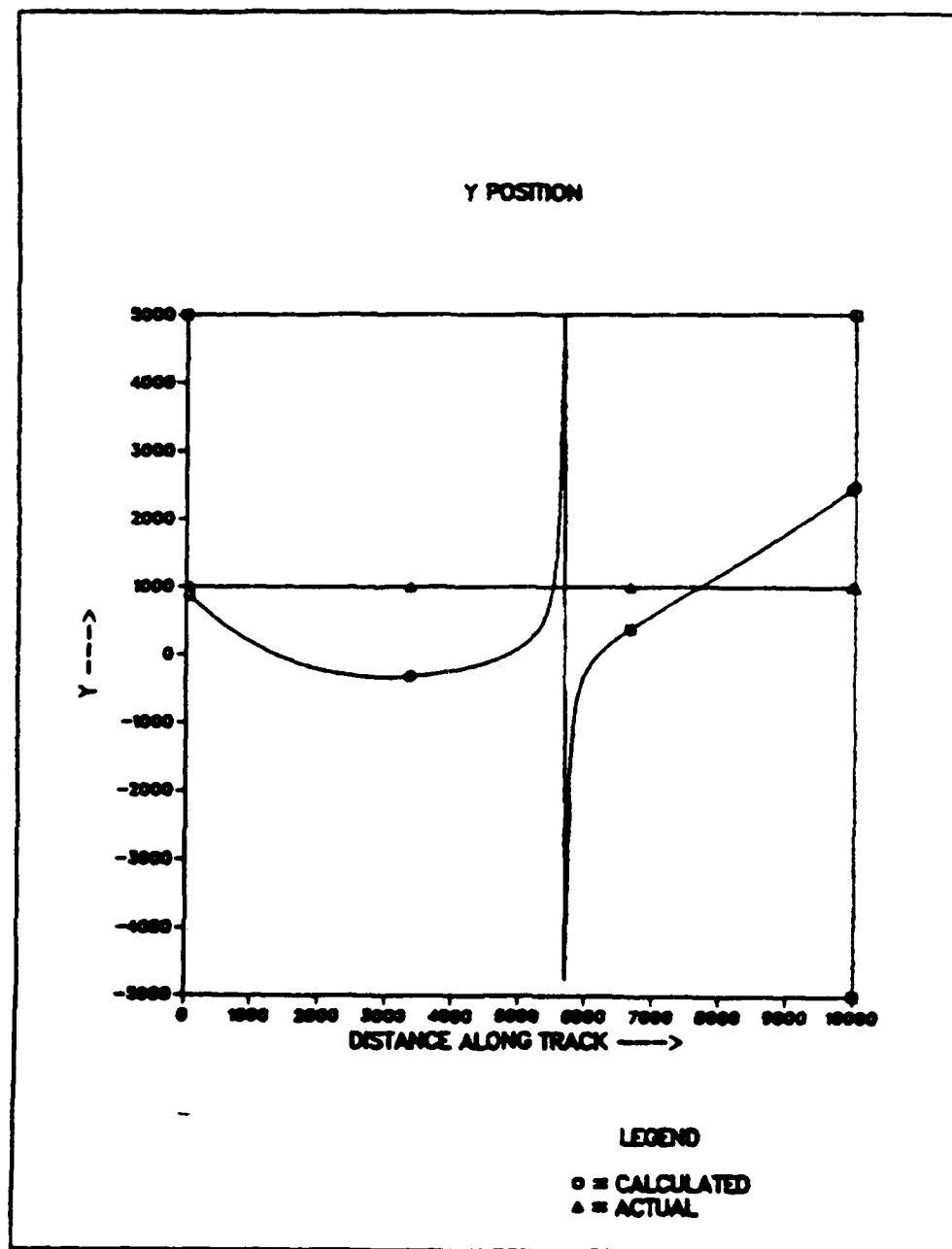


Figure 4.2 Initial Run, y position.

From the orientation of the coordinate system shown in Figure 1.2,  $z$  is in the direction of flight,  $y$  is straight down, and  $x$  is off the right side of the platform. Since

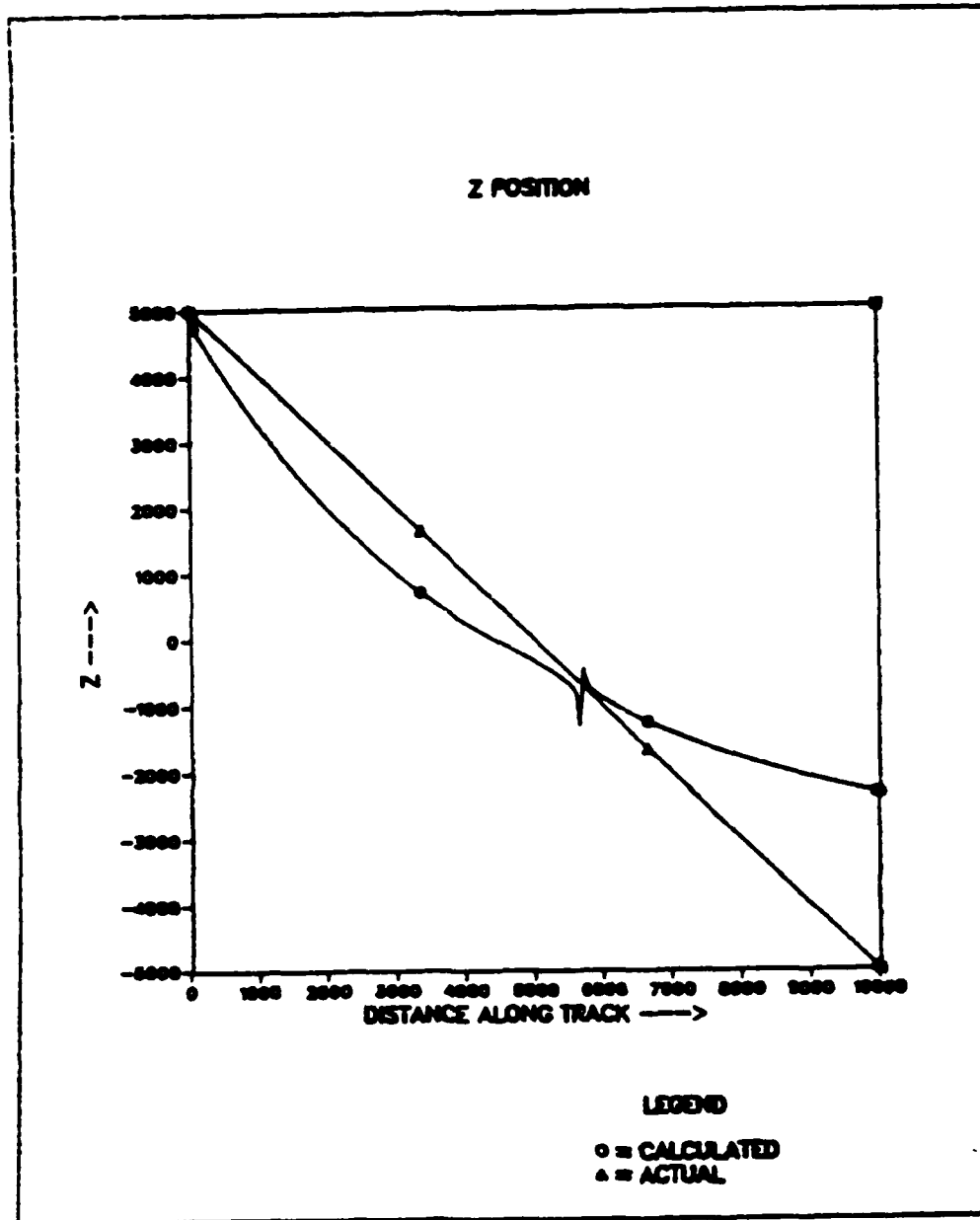


Figure 4.3 Initial Run, z position.

this thesis investigates straight line encounters only, the  $x(\text{actual})$  and  $y(\text{actual})$  coordinates will remain constant throughout any run for the coordinate orientation used. The

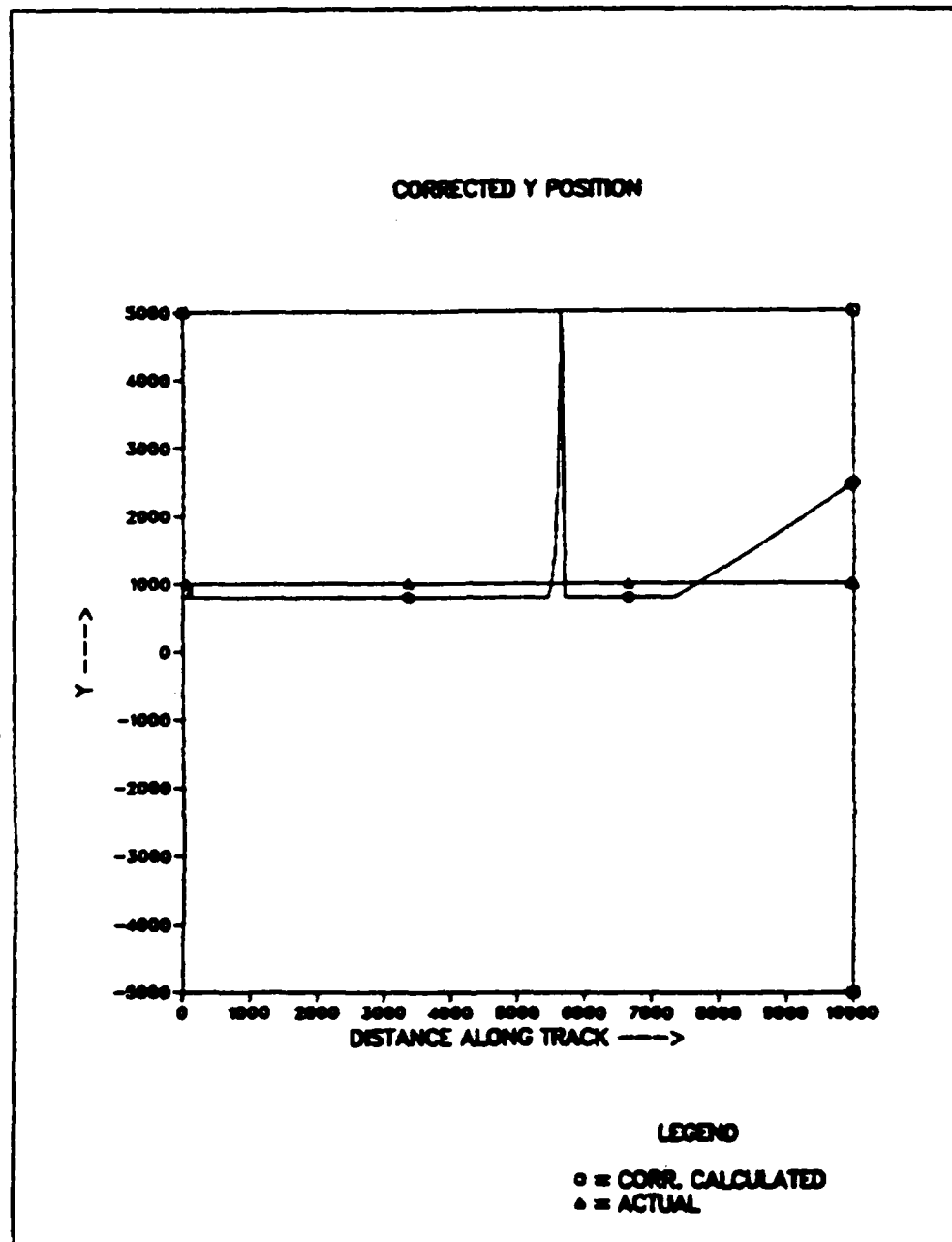


Figure 4.4 Initial Run, corrected y position.

five measurements will therefore be made with their respective x and y coordinates as constants. The z coordinate will vary. This means that for the initial pass described,

x(actual) would be constant at zero, y(actual) would be constant at 1000 feet, while z(actual) would progress from 5000 feet to -5000 feet. Figures 4.1 - 4.3 show a comparison of the actual and calculated target positions as the platform completes the initial run described earlier. It will be noted that the calculated and actual x, y, and z positions are almost identical at the start of the run. This is a coincidence. "Crossover" points such as this occur for all three coordinates simultaneously during a run, falling closer or further away from CPA, depending upon the choice of parameters.

In this initial run, it is obvious that the "worst" estimates occur for the y coordinate. This is less significant than it seems at first glance, however, as the y coordinate is the vertical separation between the platform and the target. If the target is submerged, this value is unknown, but the altitude of the platform is known. The target can be no closer to the platform than this altitude, since the target is physically unable to rise above the ocean surface. As an example, if a target depth of 200 feet is assumed, the initial y separation of 1000 feet forces the altitude in this simulation to be 800 feet. Using this value as a bound on y, it can be seen in Figure 4.4 that the y calculated position is somewhat improved. Accordingly, it seems that the particular arrangements of sensors shown in Figure 1.1 does show promise in the problem of utilizing this geometry of Multiple MAD for accurate localization purposes. Accordingly, variations of parameters were tried in order to determine what effect changing them would have. In all cases, parameters not specifically mentioned in a section will retain the values as for the initial run described above. The singularity-like behavior occurring at various places on the graphs are a result of the determinant of the denominator in the Cramer's Rule subroutine having a value close to zero.

## B. HEADING CHANGES

In this section, the localization process will be investigated as a function of heading. Compared to the initial conditions described above, the crossover points were found to be moved further out past 5000 feet prior to CPA on a heading of 0°. While a specific example of this is not shown, the behavior of the crossover points for the platform headings of 30° and 60° may be observed by comparing Figures 4.1 - 4.4 to the respective portions of Figure 4.5. The x position estimates were better for a North-South heading than for any other platform heading, although the estimates on East-West headings were also very good. For a 90° heading there are two crossover points located equidistant at 1200 feet from CPA. Calculated positions on all headings are generally good, excepting those around 60°, where the x estimates shows a large discrepancy at distances greater than 3000 feet prior to CPA. The y estimates are not significantly affected, but the z estimates are good only within ± 1200 feet of CPA. Nevertheless, even in this worst-case situation, reasonable calculated coordinates are available for localization along a significant portion of the track.

As shown in Figures 4.5 - 4.8, headings in the quadrant 0° - 90° reasonably describe what happens on any heading, as the graphs for analogous headings (60°, 120°, 240°, and 300° in this example) have similar shapes, although the orientation may differ between quadrants. These similarities are apparently due to the fact that analogous heading in quadrants 1 and 3 and quadrants 2 and 4 are in fact reciprocal headings, and so one would expect the graphs to maintain the same shape; however, the ending point of one would represent the starting point of the other. The relationship between adjacent quadrants probably exists for similar reasons.

### C. TARGET DIPOLE MOMENT CHANGES

In this section, the horizontal component of  $\vec{m}$  was oriented in the  $0^\circ$  (magnetic North) direction vice  $355^\circ$ , and the vertical component of  $\vec{m}$  was varied. The best positioning was obtained for  $\vec{m}$  oriented vertically up, i.e., no horizontal component, and an example for that case is shown in figure 4.9. Poor positioning was obtained for the vertical component of  $\vec{m}$  pointing between the horizontal and  $45^\circ$  up. The worst case shown is Figure 4.10, where  $\vec{m}$  is oriented horizontally pointing due north. With the moment oriented at an angle below the horizontal, reasonable positioning estimates were obtained. There was less variability in positioning for moments pointing below the horizontal than for those pointing above the horizontal.

The results for variations in the orientation of the target dipole moment suggests that the positioning estimates are less sensitive to moment orientation changes in the horizontal plane as compared to the vertical plane. For example, by keeping the vertical component of  $\vec{m}$  constant at an angle of  $50^\circ$  down while varying the horizontal component direction it was found that the horizontal component affected the positioning much less than variations in the vertical. Illustrated in Figure 4.11, the x estimates of position improve as the horizontal component approaches the platform heading, while the y estimates improve as the horizontal component approaches alignment with magnetic North. The latter case is not shown.

### D. CHANGES IN SENSOR SPACING

Changing the inter-sensor spacing had at most a weak effect upon the position output, even with spacing as short as 5 feet or as long as 200 feet. This would be expected in a computer simulation where sufficient precision is

available. For a spacing as great as 1000 feet some effect became noticeable. In the real world, sensor spacing would influence the localization estimates.

#### **E. ALTITUDE CHANGES**

For a straight overhead pass, positioning information appears best if a pass with a 500 to 1000 foot separation between the target and the platform is made at CPA. At greater altitudes, the accuracy suffers slightly with the increase in altitude, while at lesser ranges, usable positioning information is obtained only relatively close to CPA. For example, for a vertical separation of 400 feet, positioning data was very inaccurate at slant ranges greater than 1000 feet.

#### **F. NON-OVERHEAD PASSES**

This program gives poor results for passes that are not directly over or directly off to one side of the target. The worst situation observed in any variation is illustrated in Figure 4.12. To generate this figure, a pass was made such that the actual x coordinate was approximately equal to the actual y coordinate. The best positioning was achieved by overhead passes, but low off to the side passes can yield good results as well.

#### **G. AVERAGES**

The averages resulting from a number of runs are presented in Table I. These selected averages, covering all of the variations discussed in this chapter, show little consistency. This is probably due in part to the existence of the singularities. The variability is also a function of the limits of travel for the runs. Nevertheless, for most

TABLE I

Values of x and y Averaged over a Run

run	hdq	d	vert	horiz	avg x	avg y	avg x	avg y
1	300	500	500	500	0	42	1000	480
2	1500	500	500	500	0	-17	1000	651
3	1500	500	500	500	0	19	1000	548
4	1500	500	500	500	0	296	1000	893
5	1500	500	500	500	0	302	1000	-248
6	1500	500	500	500	0	244	1000	-185
7	1500	500	500	500	0	222	1000	-169
8	1500	500	500	500	0	326	1000	-217
9	1500	500	500	500	0	96	1000	385
10	1500	500	500	500	0	11	1000	539
11	1500	500	500	500	0	244	1000	825
12	1500	500	500	500	0	-219	1000	-167
13	1500	500	500	500	0	-10	1000	585
14	1500	500	500	500	0	26	1000	494
15	1500	500	500	500	0	-96	1000	1025
16	1500	500	500	500	0	384	1000	-532
17	1500	500	500	500	0	199	1000	-796
18	1500	500	500	500	0	-206	1000	-674
19	1500	500	500	500	0	-88	1000	-18
20	1500	500	500	500	0	199	1000	-797
21	1500	500	500	500	0	79	1000	462
22	1500	500	500	500	0	102	1000	631
23	1500	500	500	500	0	66	1000	993
24	1500	500	500	500	0	383	1000	-270
25	1500	500	500	500	0	376	1000	321
26	1500	500	500	500	0	412	900	1690
27	1500	500	500	500	0	-180	900	199
28	1500	500	500	500	0	-116	700	848
29	1500	500	500	500	0	-255	600	911
30	1500	500	500	500	0	-501	500	440
31	1500	500	500	500	0	-412	400	-423
32	1500	500	500	500	0	1147	300	-2025
33	1500	500	500	500	0	944	200	-1861
34	1500	500	500	500	0	797	100	-1665
35	1500	500	500	500	0	813	0	-1471
36	1500	500	500	500	0	-478	0	538
37	1500	500	500	500	0	345	800	492
38	1500	500	500	500	0	37	1000	466
39	1500	500	500	500	0	37	1000	461
40	1500	500	500	500	0	38	1000	470
41	1500	500	500	500	0	45	1000	490
42	1500	500	500	500	0	48	1000	500
43	1500	500	500	500	0	193	1000	759
44	1500	500	500	500	0	-166	800	662
45	1500	500	500	500	0	-238	600	1058
46	1500	500	500	500	0	-870	400	1757
47	1500	500	500	500	0	390	200	263
48	1500	500	500	500	0	108	1200	372
49	1500	500	500	500	0	219	1400	246
50	1500	500	500	500	0	266	1600	192
51	1500	500	500	500	0	313	1800	152
52	1500	500	500	500	0	410	2000	72
53	1500	500	500	500	0	-275	1000	-344
54	1500	500	500	500	0	-138	1000	140
55	1500	500	500	500	0	-226	1000	693
56	1500	500	500	500	0	-584	1000	-785
57	1500	500	500	500	0	-802	1000	-19
58	1500	500	500	500	0	332	1000	-201

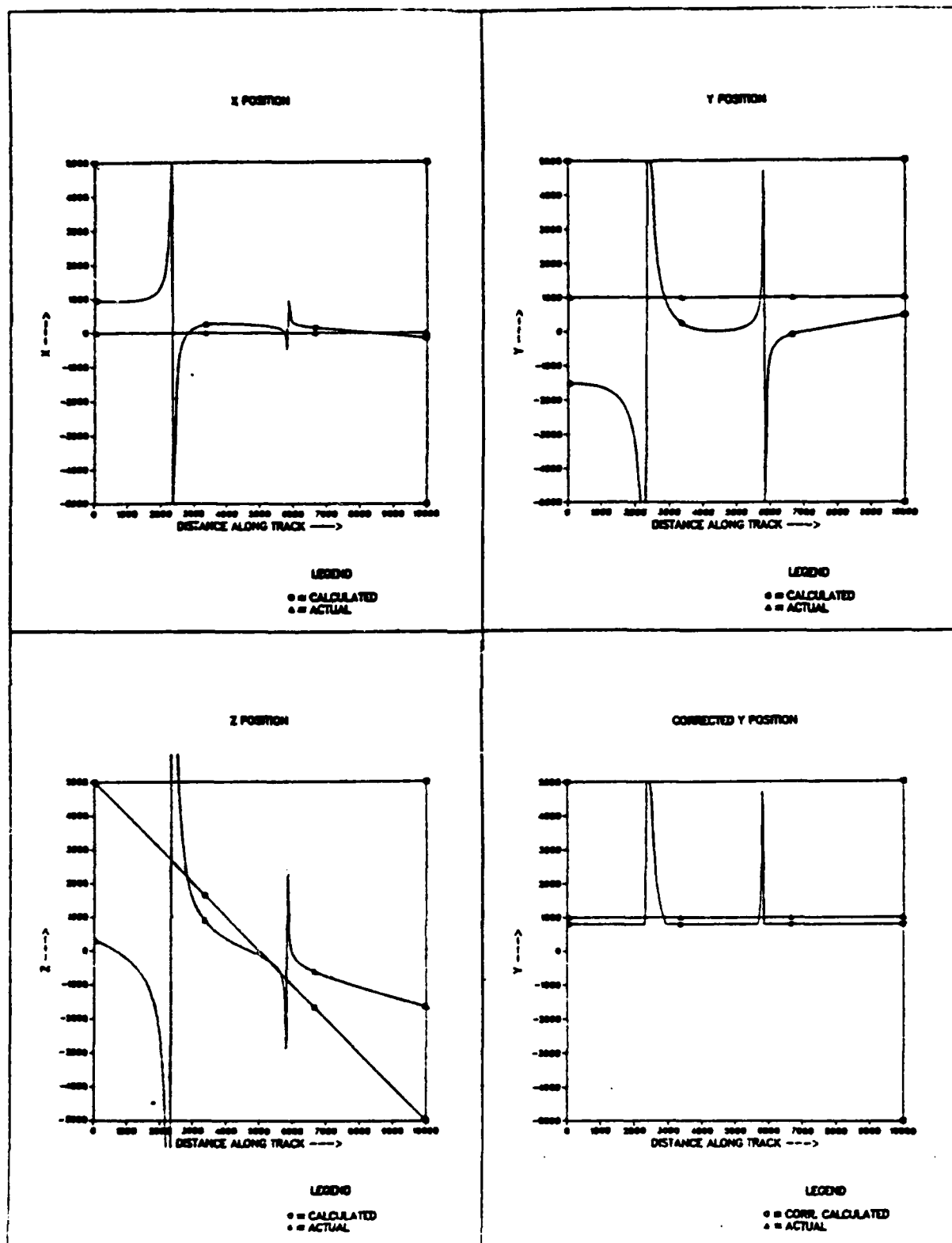


Figure 4.5 Platform Heading 60° Magnetic.

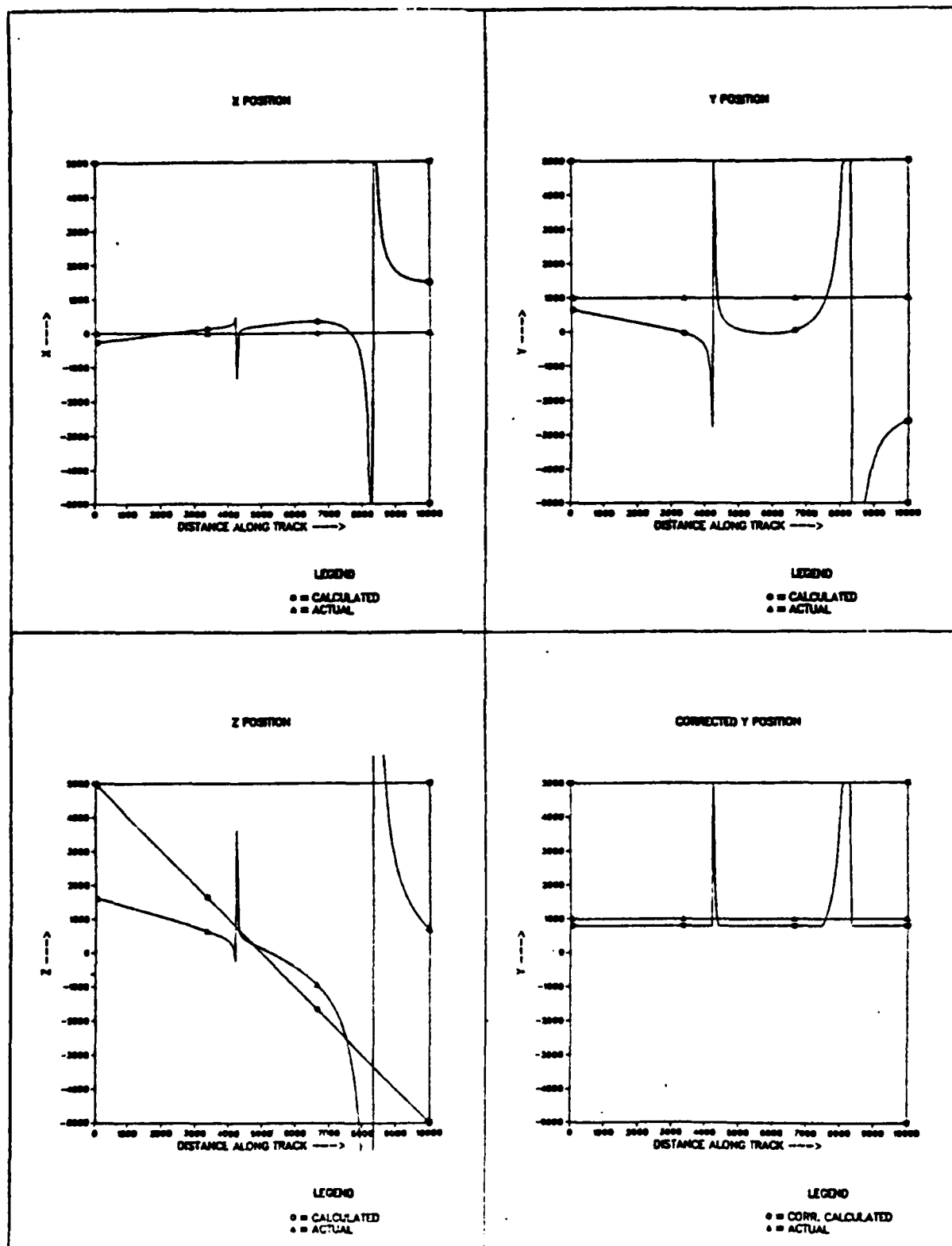


Figure 4.6 Platform Heading 120° Magnetic.

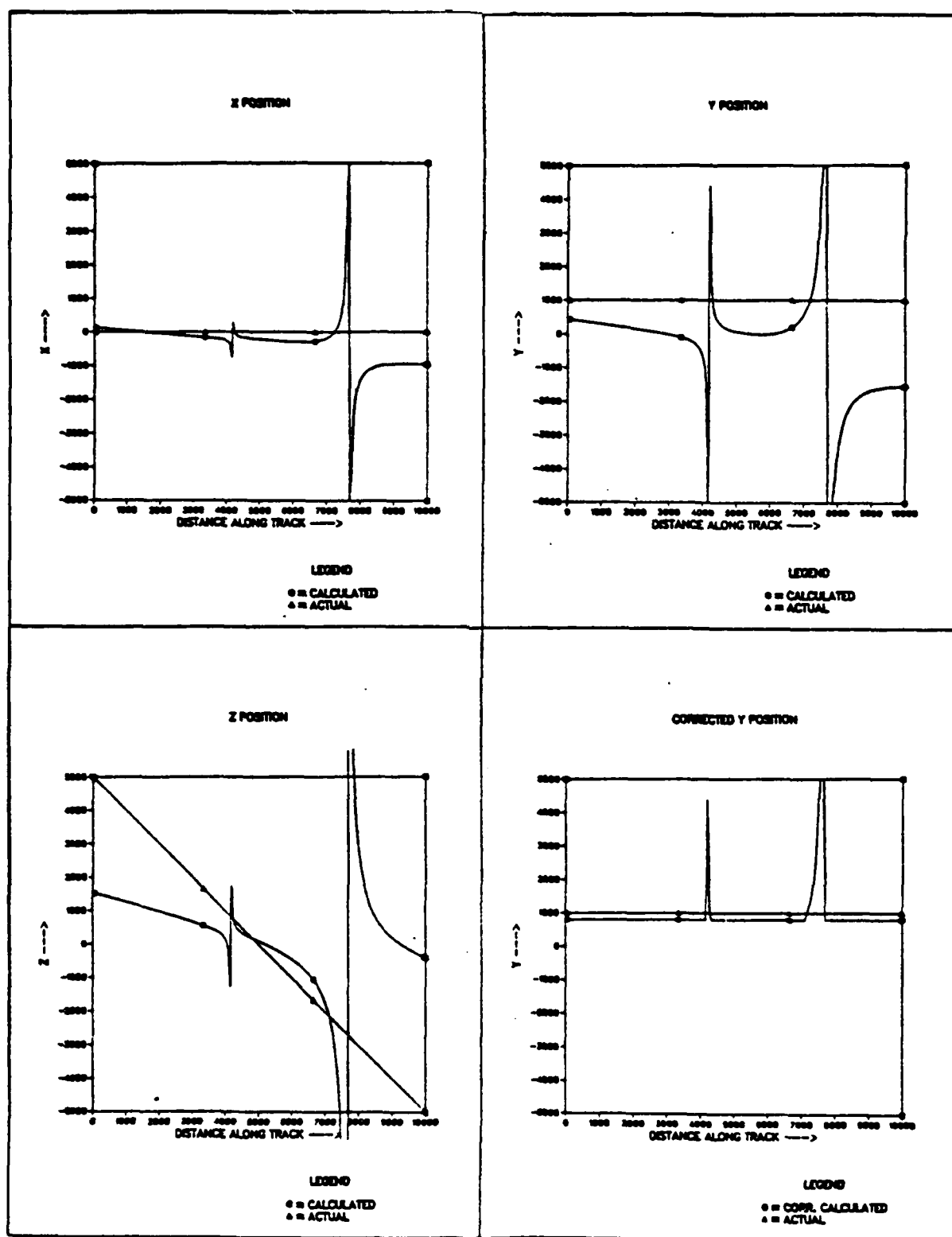


Figure 4.7 Platform Heading 240° Magnetic.

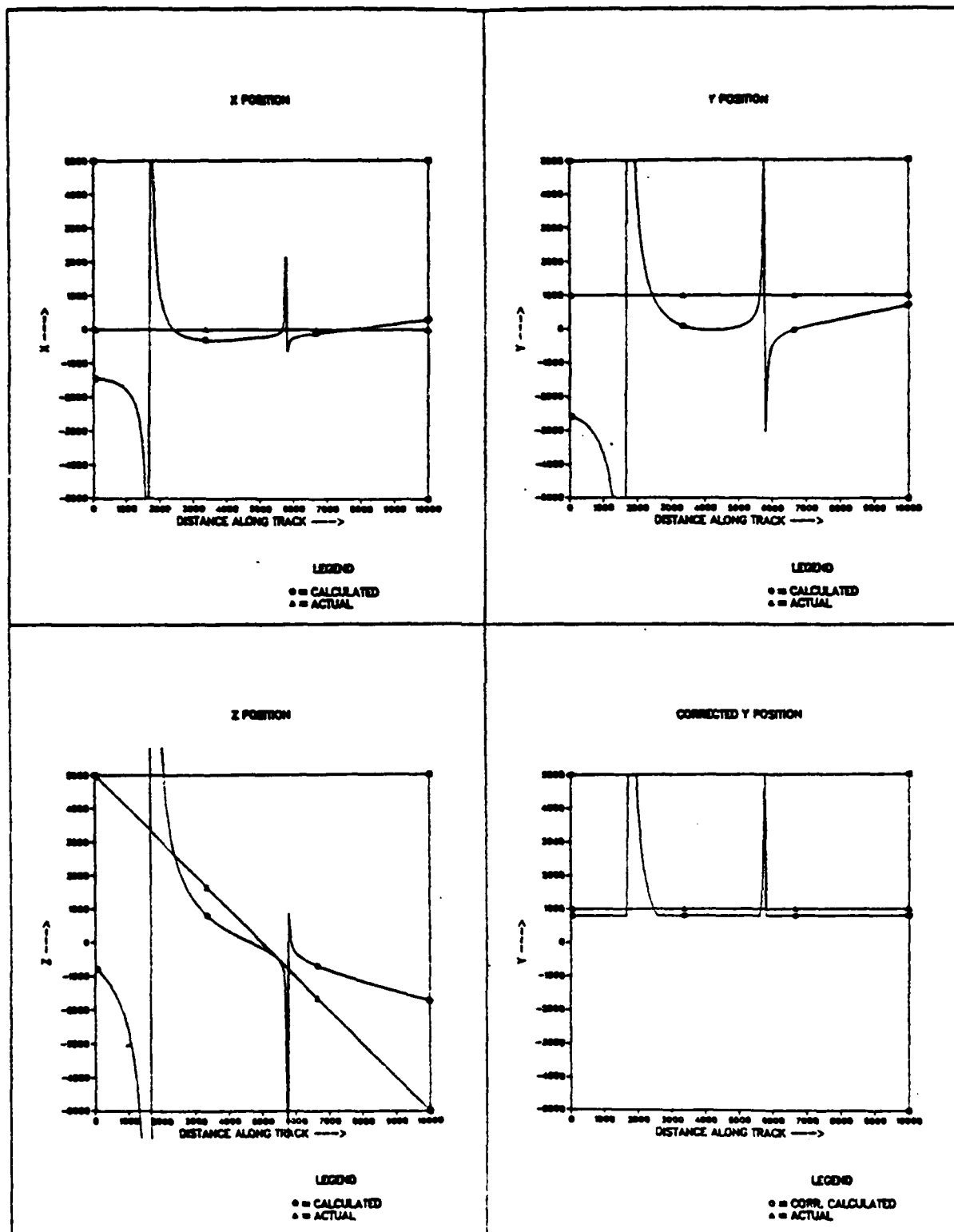


Figure 4.8 Platform Heading 300° Magnetic.

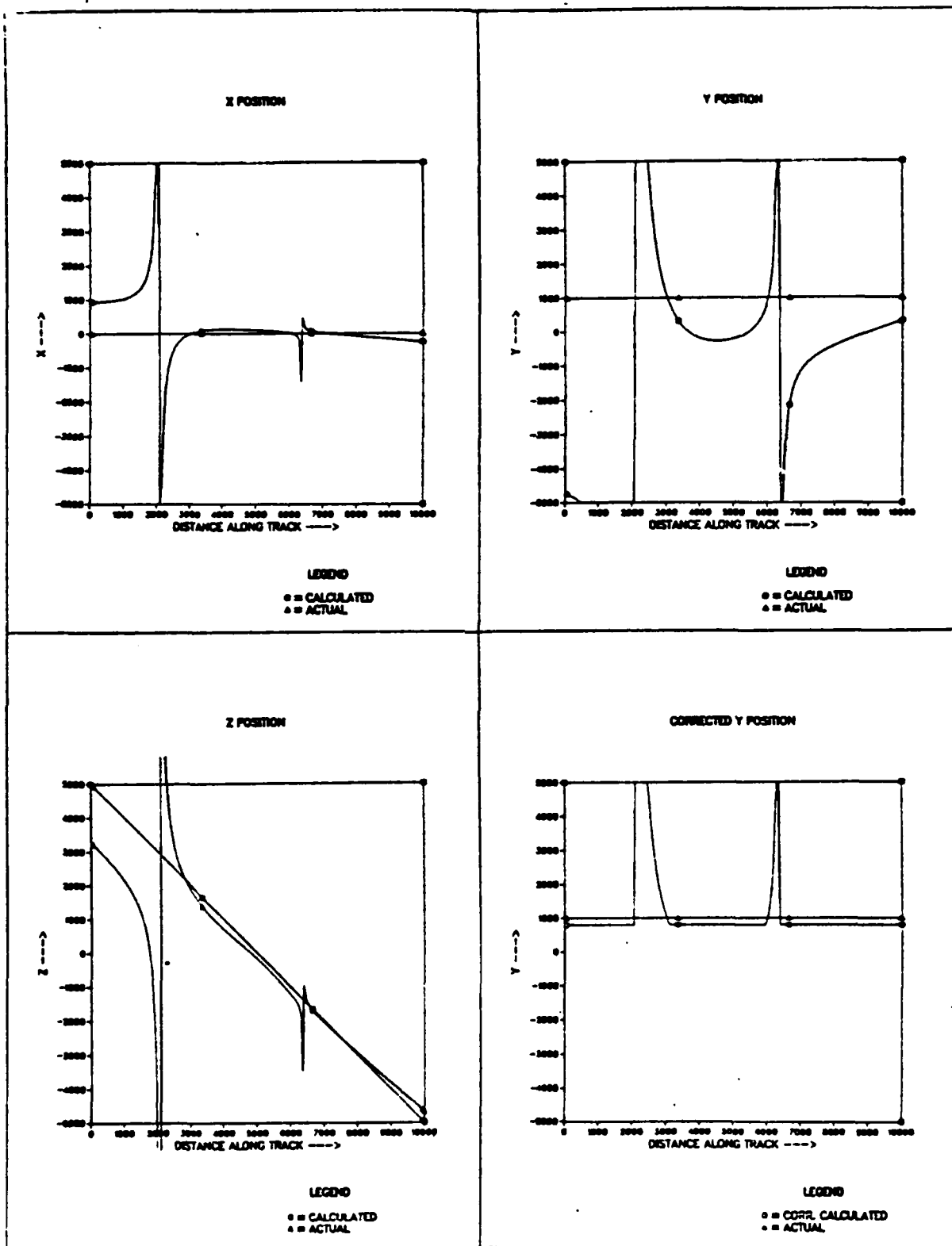


Figure 4.9  $\vec{m}$  Vertically Up.

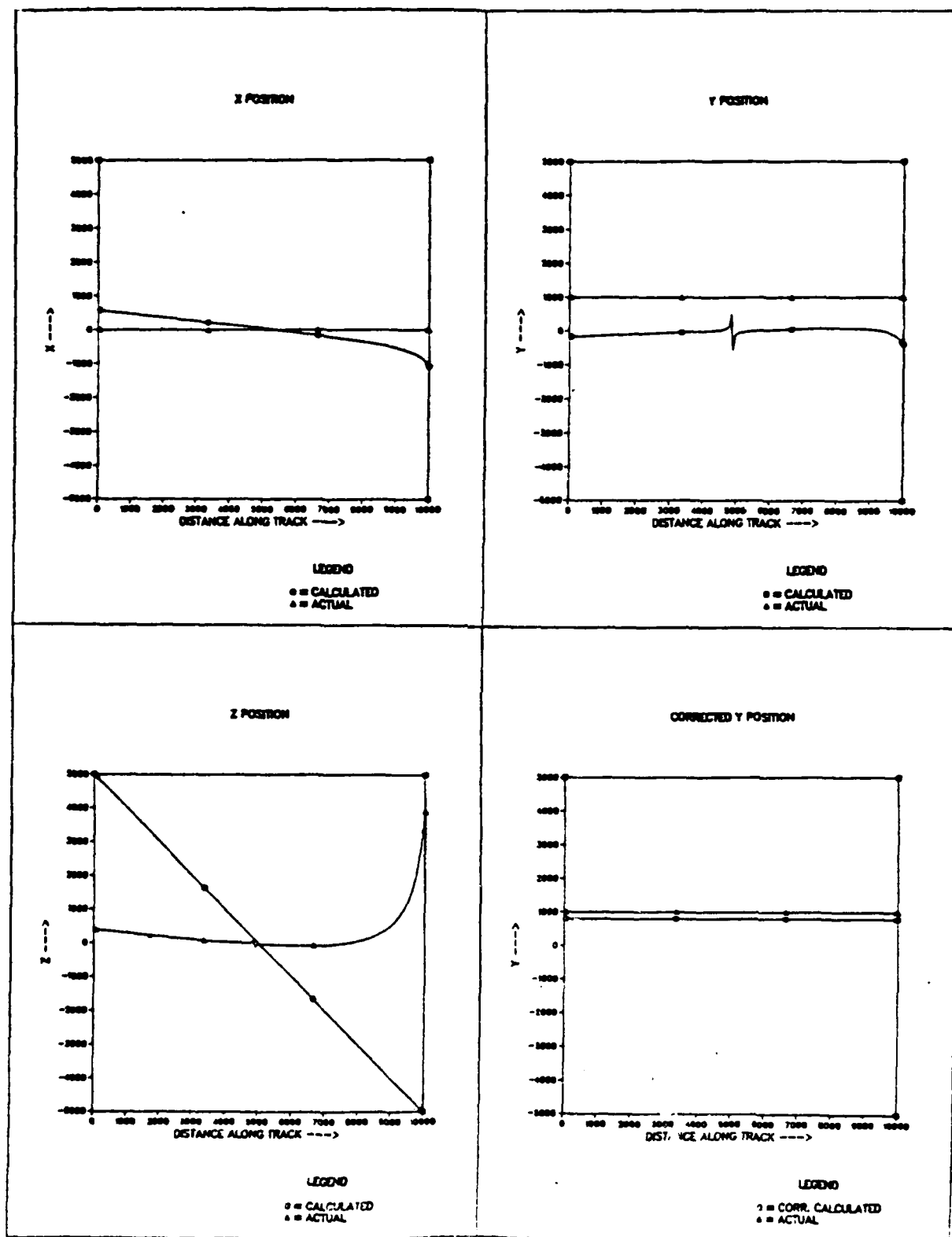


Figure 4.10  $\vec{M}$  Horizontal and Oriented to Magnetic North.

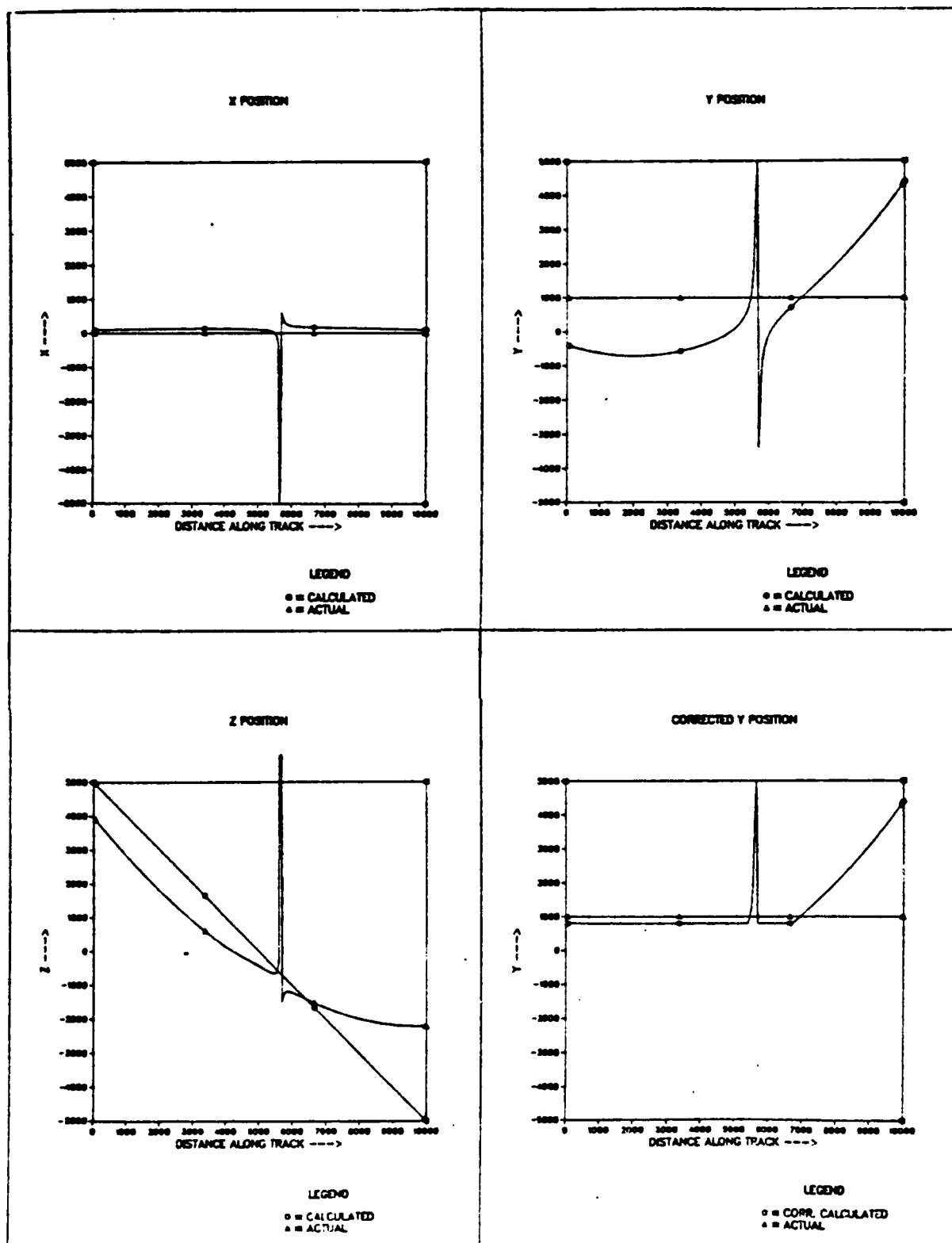


Figure 4.11  $\vec{m}$  Vert. Comp. 50° Down,  $\vec{m}$  Hor. Comp. 30° Magnetic.

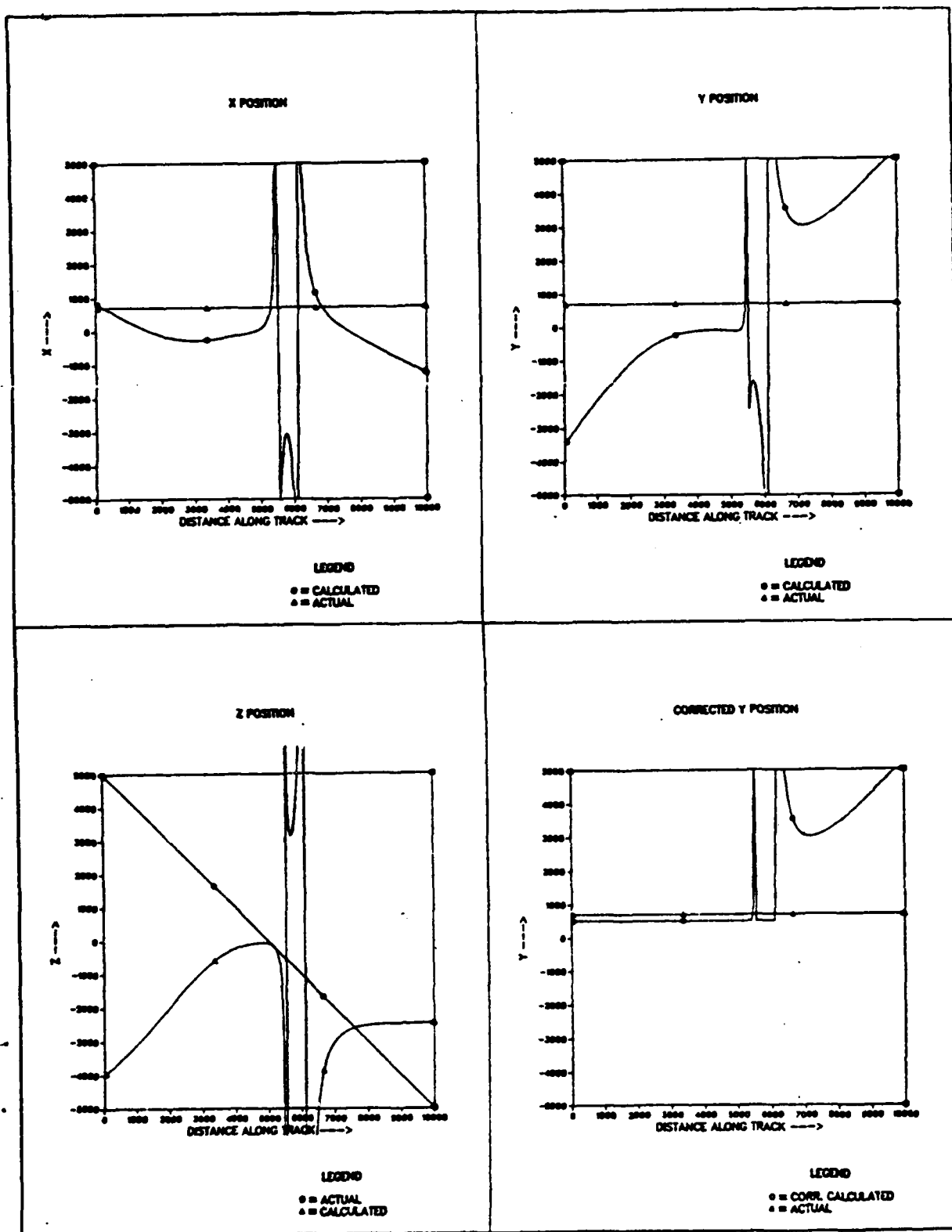


Figure 4.12 Target at 45° depres. angle rel. to platform at CPA.

cases, they do show reasonable values, and by themselves do provide limited localization data. The problem for inflight analysis would be to determine the bounds of a run in the absence of any other target positioning data.

## **H. IMPORTANCE OF CONSISTENCY**

An important observation resulting from the analysis of the graphs, including those not shown as examples in this chapter, is that the rate of change of the calculated coordinates gives some indication of the validity of the positioning data. If the x and y graphs have a slope close to zero, and if the z graph has a slope of  $-45^\circ$  for the calculated coordinate, then positioning data is likely to be comparatively accurate. If all three graphs fulfill this condition simultaneously, then positioning data appears to be usable.

## **I. IMPLEMENTATION**

The possible implementation of the process described in this thesis would be to assume a magnetic moment for the target, then run the signal data through the processing to generate positioning data, and then compare these results to those obtained by using the assumed moment to generate a signal via this simulation. If the agreement between results were good, one could assume that one had assumed the correct target moment; if not, one would assume a different moment, and go through the process again, until one had a reasonable target moment, which would be valid at least until the target changed course. Using a computer these comparisons could be made reasonably quickly, so this process might have operational possibilities.

## V. CONCLUSION

For the assumptions made, the positioning estimates are reasonable. Also, the averages taken of the three coordinates as calculated throughout the various runs show that the x calculation averages are in general at worst within 500 feet of the actual x value, while the worst y calculation averages tend to be within 1000 feet of the actual y value. The best calculated x and y values were within 100 and 200 feet, respectively, of the true values.

Trends observed were as follows:

1. It is best to fly the sensor platform directly over the target, or alternatively to have a 'distant' (between 1000 and 2000 foot) CPA off to one side while minimizing the target to platform separation in the y direction. The worst situation is when the target is at a point that, at CPA, has a depression angle of  $45^\circ$  with respect to the platform.
2. Best vertical separations are those that will yield a 500 to 1000 foot vertical distance between target and platform. Short vertical separations should be avoided if good localization is desired.
3. Best results are obtained if headings are northerly or southerly. Poor results are achieved with headings close to  $60^\circ$ ,  $120^\circ$ ,  $240^\circ$ , and  $300^\circ$ . East-West headings, while not as good as North-South, do provide good positioning data close to CPA.
4. Good results may be expected if there is a large vertical moment, especially if it is vertically up. Poor positioning results are obtained with this simulation if the moment has a large horizontal component.

5. Results are slightly better if the target moment is lined up with either the axis of flight or with the earth's field, although this effect is often dominated by the more gross effects caused by the other variables.

A suggested approach for further study is to inject noise into the simulation in order to see how robust it is in the accuracy of the position calculations. If the results remain reasonable, this approximation or an altered form of it may one day have real-world applicability.

# COMPUTER PROGRAM FOR PLOT OUTPUT

[illegible]

```

MZ = 5.D0*(CCOS(RALFA))*(DCOS(RBETA))
EX = -(DCOS(RTHETA))*(DSIN(RPHEE))
EY = DSIN(RTHETA)
EZ = (CCOS(RTHETA))*(DCOS(RPHEE))
G = (MX*EX)+(MY*EY)+(MZ*EZ)
V1 = (3.D0*MX*EX) - G
V2 = 3.D0*((MX*EY)+(MY*EX))
V3 = (3.D0*MY*EY) - G
V4 = 3.D0*((MY*EZ)+(MZ*EY))
V5 = (3.D0*MZ*EZ) - G
V6 = 3.D0*((MX*EZ)+(MZ*EX))

```

THE INITIAL POSITION OF SENSOR 1, AS WELL AS THE SENSOR SPACING  
DISTANCE "D" IS SET HERE - IF A CHANGE IS DESIRED, THE PROGRAM  
MUST BE ALTERED AT THIS POINT.

```

X(1) = 0.D0
Y(1) = -1000.D0
Z(1) = -5000.D0
D = 50.D0
COB(1) = 0.C
COA(1) = 5000.0
COB(2) = 10000.0
COA(2) = 5000.0
COB(3) = 10000.0
COA(3) = -5000.0

```

THE INITIAL POSITIONS OF SENSORS 2 - 5 ARE CALCULATED HERE.

```

X(2) = X(1) - D
Y(2) = Y(1) - D
X(3) = X(1)
Y(3) = Y(1)
X(4) = X(1) + D
Y(4) = Y(1) + D
X(5) = X(1)
Y(5) = Y(1)
Z(2) = Z(1)
Z(3) = Z(1)
Z(4) = Z(1)
Z(5) = Z(1)

```

THE ACTUAL SIGNAL, BASED ON THE DIPOLE EQUATION, TO BE RECEIVED  
AT EACH OF THE FIVE SENSORS IS CALCULATED AT THIS POINT.

```

DO 20 J=1,5
RG = DSQRT((X(J)**2) + (Y(J)**2) + (Z(J)**2))
DOTME = (MX*EX)+(MY*EY)+(MZ*EZ)

```

```

M1000490
M1000500
M1000510
M1000520
M1000530
M1000540
M1000550
M1000560
M1000570
M1000580
M1000590
M1000600
M1000610
M1000620
M1000630
M1000640
M1000650
M1000660
M1000670
M1000680
M1000690
M1000700
M1000710
M1000720
M1000730
M1000740
M1000750
M1000760
M1000770
M1000780
M1000790
M1000800
M1000810
M1000820
M1000830
M1000840
M1000850
M1000860
M1000870
M1000880
M1000890
M1000900
M1000910
M1000920
M1000930
M1000940
M1000950
M1000960

```

```

DCTMR = (MX*X(J)) + (MY*Y(J)) + (MZ*Z(J))
DCTRE = (X(J)*EX) + (Y(J)*EY) + (Z(J)*EZ)
TERM1 = (-DCTMR) * (RG**2)
ANUM(J) = 3.0 * DCTMR * DCTRE
TERM3 = 1.0 * (RG**5)
S(J) = TERM3 * (ANUM(J))
RNG(J) = RG
20 CONTINUE

```

DIFFERENCES OF RECEIVED SIGNAL ARE TAKEN, IN ORDER TO ELIMINATE SQUARE AND HIGHER ORDER TERMS. THE DENOMINATOR IS ASSUMED TO BE THE SAME FOR THIS APPROXIMATION.

```

S2S3 = S(2) - S(3)
S2S5 = S(2) - S(5)
S3S1 = S(3) - S(1)
S5S1 = S(5) - S(1)
S3S4 = S(3) - S(4)
S5S4 = S(5) - S(4)

```

THE RATIOS OF THE ABOVE DIFFERENCES ARE TAKEN IN ORDER TO ELIMINATE THE FIFTH-ORDER TERM IN THE DENOMINATOR.

```

A1 = S2S3/S2S5
A2 = S3S1/S5S1
A3 = S3S4/S5S4

```

EQUATION 3.1 COEFFICIENTS

```

C1 = (A1*(V2+(2.00*V1))) - (V2-(2.00*V1))
C2 = (A1*((2.00*V3)+V2)) - ((2.00*V3)-V2)
C3 = (A1*((V4+V6)) - (V4-V6)
K1 = ((V1-V3) - (A1*(V1-V3))) * D

```

EQUATION 3.2 COEFFICIENTS

```

C4 = (A2*2.00*V1) + (2.00*V1)
C5 = (A2*V2) + V2
C6 = (A2*V6) + V6
K2 = (V1 - (A2*V1)) * D

```

EQUATION 3.2 COEFFICIENTS

```

C7 = (A3*(V6+(2.00*V1))) - (V6-(2.00*V1))
C8 = (A3*(V4+V2)) - (V4-V2)
C9 = (A3*((2.00*V5)+V6)) - ((2.00*V5)-V6)
K3 = ((V1-V5) - (A3*(V1-V5))) * D

```

M1000970  
M1000980  
M1000990  
M1001000  
M1001010  
M1001020  
M1001030  
M1001040  
M1001050  
M1001060  
M1001070  
M1001080  
M1001090  
M1001100  
M1001110  
M1001120  
M1001130  
M1001140  
M1001150  
M1001160  
M1001170  
M1001180  
M1001190  
M1001200  
M1001210  
M1001220  
M1001230  
M1001240  
M1001250  
M1001260  
M1001270  
M1001280  
M1001290  
M1001300  
M1001310  
M1001320  
M1001330  
M1001340  
M1001350  
M1001360  
M1001370  
M1001380  
M1001390  
M1001400  
M1001410  
M1001420  
M1001430  
M1001440

```

C
C
C   THE COEFFICIENTS ARE SENT TO THE CRAMER'S RULE SUBROUTINE.
      CALL SUBMAT(C1,C2,C3,K1,C4,C5,C6,K2,C7,C8,C9,K3,XX,YY,ZZ)
      IF (XX.LT.5000.0) GO TO 80
      XX = 5000.0
      GO TO 81
80  IF (XX.GT.-5000.0) GO TO 81
      XX = -5000.0
      RX(N) = X(I)
81  CX(N) = XX
      IF (YY.LT.5000.0) GO TO 82
      YY = 5000.0
      GO TO 83
82  IF (YY.GT.-5000.0) GO TO 83
      YY = -5000.0
      RY(N) = Y(I)
83  CY(N) = YY
      RZ(N) = Z(I) + 5000.0
      RR(N) = Z(I)
      CZ(N) = ZZ
      N = N + 1
      ZEIT(N) = N
      IF (Z(I).GE.5000.00) GO TO 40
C
C   THE PLATFORM IS ADVANCED ONE TIME STEP IN POSITION. IF A DIFFERENT
C   SIZE STEP IS DESIRED, IT MUST BE ADJUSTED HERE.
      Z(I) = Z(I) + 50.00
      GO TO 30
C
C   THIS IS THE PLOTTING ROUTINE.
40  DC 97 K=1,200
      RX(K) = -RX(K)
      RY(K) = -RY(K)
      RR(K) = -RR(K)
      CX(K) = -CX(K)
      CY(K) = -CY(K)
      CZ(K) = -CZ(K)
      HOCH = -Y(I) - 200.0
      IF (CY(K).LT.HOCH) GO TO 96
      YC(K) = CY(K)
      GO TO 97
96  YC(K) = HOCH
      CCNT INUE
57  CALL TEK618
      CALL PLOTD(COB,COA,3,.FALSE., 'LINLIN', ' $', 'X POSITIONS', 'DISTANCE'
M1001450
M1001460
M1001470
M1001480
M1001490
M1001500
M1001510
M1001520
M1001530
M1001540
M1001550
M1001560
M1001570
M1001580
M1001590
M1001600
M1001610
M1001620
M1001630
M1001640
M1001650
M1001660
M1001670
M1001680
M1001690
M1001700
M1001710
M1001720
M1001730
M1001740
M1001750
M1001760
M1001770
M1001780
M1001790
M1001800
M1001810
M1001820
M1001830
M1001840
M1001850
M1001860
M1001870
M1001880
M1001890
M1001900
M1001910
M1001920

```





COMPUTER PROGRAM FOR NUMERICAL OUTPUT

```

THIS PROGRAM DOES THE SAME JOB AS THE ONE IN APPENDIX A, BUT THE
OUTPUT IS IN NUMERICAL FORM. IN ADDITION TO THE COMPARATIVE
POSITIONS, THE ACTUAL COEFFICIENTS OF THE EQUATIONS GOING INTO
THE CRAMER'S RULE SUBROUTINE ARE LISTED, AS ARE RATIOS OF THEM TO
ESTABLISH THAT THEY ARE INDEED LINEARLY INDEPENDENT. THE EXPECTED
SIGNAL STRENGTH AT EACH SENSOR IS ALSO COMPARED TO THE EXPECTED
SIGNAL STRENGTH USING THE RANGE TO SENSOR 1 AS THE COMMON
DENOMINATOR FOR THE APPROXIMATION. NOTE THAT THE POSITIONS GIVEN
AS THE SOLUTION HAVE THE TARGET, NOT THE PLATFORM, AS THE ORIGIN,
AND THAT SAID POSITIONS ARE THE PLATFORM'S POSITION.

```

```

      REAL*8 MX1,MY,MZ,EX,EY,EZ,X,Y,Z,D,S,RG,S2S3,S2S5,G,PI,RADN,RTHETA,
      *RPHEE,S3S1,S3S4,A1,A2,A3,C1,C2,C3,C4,C5,C6,C7,C8,C9,K1,K2,K3,
      *S5S4,V1,V2,V3,V4,V5,V6,RALFA,RBETA
      REAL K1K2,K1K3,K2K3
      DIMENSION X(5),Y(5),Z(5),S(5),RNG(5),ANUM(5)

```

```

THE SAME PARAMETERS AS FOR THE PROGRAM IN APPENDIX A ARE ENTERED
HERE. THE ONLY DIFFERENCE IS THAT BETA, THE DIPOLE HORIZONTAL
COMPONENT, IS INSERTED IN DEGREES COUNTER-CLOCKWISE FROM THE
PLATFORM HEADING. ALL PARAMETER CHANGES IN THIS PROGRAM ARE NON-
INTERACTIVE, AND MUST BE CHANGED IN THE PROGRAM ITSELF.

```

```

      PHEE = 30.
      THETA = 70.
      ALFA = 50.
      BETA = 35.
      PI = 4.D0 * DATAN(1.D0)
      RADN = PI / 180.D0
      RTHETA = THETA * RADN
      RPHEE = PHEE * RADN
      RALFA = ALFA * RADN
      RBETA = BETA * RADN
      MX = (-5.D0)*(DCOS(RALFA))*(DSIN(RBETA))
      MY = 5.D0*(DSIN(RALFA))
      MZ = 5.D0*(DCOS(RALFA))*(DCOS(RBETA))
      EX = -(DCOS(RTHETA))*(DSIN(RPHEE))
      EY = DSIN(RTHETA)
      EZ = (DCOS(RTHETA))*(DCOS(RPHEE))
      VG1 = (MX*EX)+(MY*EY)+(MZ*EZ)
      V2 = (3.D0*(MX*EX)) - G
      V3 = (3.D0*(MY*EY)) - G
      V4 = (3.D0*(MZ*EZ)) - G
      V5 = (3.D0*(MX*EZ)) - G

```

```

C
C
C
      V6 = 3.00 * ((MX*EZ)+(MZ*EX))
      AS IN THE OTHER PROGRAM, SENSOR 1 INITIAL POSITION AND THE SENSOR
      SPACING IS SET AT THIS POINT.
      X(1) = 0.00
      Y(1) = -1000.00
      Z(1) = -5000.00
      D = 50.00
      X(2) = X(1) - D
      X(3) = X(1) - D
      X(4) = X(1)
      X(5) = X(1) + D
      Y(2) = Y(1)
      Y(3) = Y(1)
      Y(4) = Y(1)
      Y(5) = Y(1)
      Z(2) = Z(1)
      Z(3) = Z(1)
      Z(4) = Z(1)
      Z(5) = Z(1)
      DO 20 J=1,5
      RG = DSQR(((X(J)**2) + (Y(J)**2) + (Z(J)**2))
      DOTIME = (MX*EX)+((MY*EY)+(MZ*EZ))
      DOTMR = (MX*X(J))+(MY*Y(J))+(MZ*Z(J))
      DOTRE = (X(J)*EX)+(Y(J)*EY)+(Z(J)*EZ)
      TERM1 = (-DOTIME)*(RG**2)
      TERM2 = 3.0*DOTMR*DOTRE
      ANUM(J) = TERM1 + TERM2
      TERM3 = 1.08 / (RG**5)
      S(J) = TERM3 * (ANUM(J))
      RNC(J) = RG
      CCNT INUE
      AVRG = 1.08 / (AVRNG**5)
      DNOM = ANUM(1) * DNOM
      S1 = ANUM(1) * DNOM
      S2 = ANUM(2) * DNOM
      S3 = ANUM(3) * DNOM
      S4 = ANUM(4) * DNOM
      S5 = ANUM(5) * DNOM
      APP2 = S2 - S3
      APP25 = S2 - S5
      APP31 = S3 - S1
      APP51 = S5 - S1
      APP34 = S3 - S4
      APP54 = S5 - S4
      1 FORMAT (10X,'ACTUAL',8X,3F10.2)
      70 FORMAT (10X,'EQNS',25X,'X',9X,'Y',9X,'Z')

```

```

M1100490
M1100500
M1100510
M1100520
M1100530
M1100540
M1100550
M1100560
M1100570
M1100580
M1100590
M1100600
M1100610
M1100620
M1100630
M1100640
M1100650
M1100660
M1100670
M1100680
M1100690
M1100700
M1100710
M1100720
M1100730
M1100740
M1100750
M1100760
M1100770
M1100780
M1100790
M1100800
M1100810
M1100820
M1100830
M1100840
M1100850
M1100860
M1100870
M1100880
M1100890
M1100900
M1100910
M1100920
M1100930
M1100940
M1100950
M1100960

```

```

71 FORMAT (1, USED, 24X, 'PUS', 7X, 'POS', 7X, 'POS')
60
S2S3 = S(2) - S(3)
S2S5 = S(2) - S(5)
S3S1 = S(3) - S(1)
S3S5 = S(3) - S(5)
S3S4 = S(3) - S(4)
S5S4 = S(5) - S(4)
A1 = S2S3/S2S5
A2 = S3S1/S3S5
A3 = S3S4/S3S5
C1 = (A1*(V2+(2.D0*V1)) - (V2-(2.D0*V1)))
C2 = (A1*(2.D0*V3)+V2) - ((2.D0*V3)-V2)
C3 = (A1*(V4+V6)) - (V4-V6)
K1 = (V1-V3) - (A1*(V1-V3)) * D
C4 = (A2*2.D0*V1) + (2.D0*V1)
C5 = (A2*V2) + V2
C6 = (A2*V6) + V6
K2 = (V1 - (A2*V1)) * D
C7 = (A3*(V6+(2.D0*V1)) - (V6-(2.D0*V1)))
C8 = (A3*(V4+V2)) - (V4-V2)
C9 = (A3*(2.D0*V5)+V6) - ((2.D0*V5)-V6)
K3 = ((V1-V5) - (A3*(V1-V5))) * D

THE BELOW LISTED VARIABLES ARE THE RATIOS OF THE COEFFICIENTS
USED TO SHOW LINEAR INDEPENDENCE OF THE THREE EQUATIONS.

K1K2 = K1/K2
K1K3 = K1/K3
K2K3 = K2/K3
C1C4 = C1/C4
C2C5 = C2/C5
C3C6 = C3/C6
C1C7 = C1/C7
C2C8 = C2/C8
C3C9 = C3/C9
C4C7 = C4/C7
C5C8 = C5/C8
C6C9 = C6/C9
WRITEE (6,60)
WRITEE (6,60)
WRITEE (6,60)
WRITEE (6,60)
110 FORMAT (1, SENSOR, 7X, 'SLANT', 8X, 'SENSED', 8X, 'CALCULATED', 10X, '|', 1M10101400
*1X, 'EQUATION', 4X, 'CONSTANT', 8X, 'X', 11X, 'Y', 11X, 'Z')
111 FORMAT (1, NUMBER, 7X, 'RANGE', 8X, 'SIGNAL', 10X, 'SIGNAL', 12X, '|', 12X, M110101430

```

[illegible]

```

REAL*8 AX,AY,AZ,AA,BX,BY,BZ,BB,CX,CY,CZ,CC,XX,YY,ZZ,DD
7  FORMAT ('+',26X,'MATRIX CANNOT BE CALCULATED.!',
DD = AX*((BY*CZ)-(BZ*CY)) - BX*((AY*CZ)-(AZ*CY)) + CX*((AY*BZ)-(AZ*
**BY))
IF (DD.NE.C.00) GO TO 98
WRITE (6,7)
GO TO 99
98  XX = (AA*((BY*CZ)-(BZ*CY)) - BB*((AY*CZ)-(AZ*CY)) + CC*((AY*BZ)-(
*Z*BY)))/DD
YY = (AX*((BB*CZ)-(BZ*CC)) - BX*((AA*CZ)-(AZ*CC)) + CX*((AA*BZ)-(
*Z*BB)))/DD
ZZ = (AX*((BY*CC)-(BB*CY)) - BX*((AY*CC)-(AA*CY)) + CX*((AY*BB)-(
*A*BY)))/DD
WRITE (6,2) XX,YY,ZZ
2  FORMAT (10X,'CALCULATED',4X,3F10.2)
60  WRITE (6,60)
99  FORMAT ('+',
END
MI101930
MI101940
MI101950
MI101960
MI101970
MI101980
MI101990
MI102000
MI102010
MI102020
MI102030
MI102040
MI102050
MI102060
MI102070
MI102080
MI102090
MI102100
MI102110

```

# **APPENDIX C** **EXAMPLE OUTPUT OF APPENDIX B**

An example of the output of the program in Appendix B is shown below. The total output for a single time step is presented.

SENSOR NUMBER	SLANT RANGE	SENSED SIGNAL	CALCULATED SIGNAL
1	5050.0	0.6054D-04	0.6054E-04
2	5060.1	0.1596D-03	0.1612E-03
3	5050.2	0.2682D-04	0.2683E-04
4	5099.0	0.3940D-04	0.4135E-04
5	5050.2	0.9366D-04	0.9368E-04

ECLATION	TRUE	APPROXIMATE
S2-S3	0.1327C-03	0.1343E-03
S2-S5	0.6590C-04	0.6748E-04
S3-S1	-0.3372C-04	-0.3371E-04
S5-S1	0.3312C-04	0.3314E-04
S3-S4	-0.1258C-04	-0.1452E-04
S5-S4	0.5426C-04	0.5233E-04

EQNS USED	X POS	Y POS	Z POS
1 2 3	0.0	-1000.00	-4950.00
-----	-----	-----	-----
ACTUAL	0.0	-1000.00	-4950.00
CALCULATED	-60.98	-870.83	-4739.97

The first five rows of data above are for the appropriate "sensor" as indicated, the slant range from that sensor to the target, the received signal as generated by equation 2.5 and the signal that would be generated using the approximation described in Chapter 3 to linearize the problem. The next six rows show the results of taking the differences between the received and calculated (for comparison purposes only) signals, listed under the headings of TRUE and APPROXIMATE, respectively. The final two lines show the actual coordinates of the platform relative to the target (the coordinate transformation has not been done at this point) as compared to the calculated position. These are the points used by the program in Appendix A to plot the graphs after the coordinate transformation is completed.

The second section of the output is shown below.

EQUATION NUMBER	CONSTANT	X COEFFICIENT	Y COEFFICIENT	Z COEFFICIENT
1	0.500+03	-0.300+02	-0.920+01	0.200+01
2	-0.580+03	0.140+00	0.130+00	0.540+01
3	-0.850+02	-0.210+01	-0.190+02	0.350+01

RATIO				
1/2	-0.13E+01	-0.22E+03	-0.71E+02	0.30E+02
1/3	-0.58E+01	0.14E+02	0.49E+00	0.50E+00
2/3	0.44E+01	-0.65E-01	-0.69E-02	0.15E-01

The first three lines of the output represent the coefficients of the equations 3.6 - 3.8 in the form of  $CONSTANT = X \text{ COEFF}(x) + Y \text{ COEFF}(y) + Z \text{ COEFF}(z)$ . In order to determine the linear independence of these equations, the ratios of the coefficients are taken in pairs. Since it may be seen from the last three lines of the output that the ratios of the constants and coefficients differ significantly for all three equations, it can be concluded that the equations are linearly independent. This holds true throughout any given run, which may be verified by printing out all time steps for that run.

APPENDIX D  
CRAMER'S RULE

A. GENERAL

Cramer's Rule, a method for solving systems of linear equations in two or more unknowns, states that each unknown can be expressed as the ratio of two determinates. The general form of a solution is shown below.

$$Ax+By+Cz=0$$

$$Ex+Fy+Gz=H$$

$$Ix+Jy+Kz=L$$

$$D = \begin{vmatrix} A & B & C \\ E & F & G \\ I & J & K \end{vmatrix}$$

$$x = \begin{vmatrix} 0 & B & C \\ H & F & G \\ L & J & K \end{vmatrix} / D$$

$$y = \begin{vmatrix} A & 0 & C \\ E & H & G \\ I & L & K \end{vmatrix} / D$$

$$z = \begin{vmatrix} A & B & 0 \\ E & F & H \\ I & J & L \end{vmatrix} / D$$

B. EXAMPLE

The following example was taken from [Ref. 4]. Solve:

$$3x-2y+2z=7$$

$$x+y+z=6$$

$$2x-y-2z=2$$

Let D be the denominator.

$$D = \begin{vmatrix} 3 & -2 & 2 \\ 1 & 1 & 1 \\ 2 & -1 & -2 \end{vmatrix} = -17$$

$$x = \frac{\begin{vmatrix} 7 & -2 & 2 \\ 6 & 1 & 1 \\ 2 & -1 & -2 \end{vmatrix}}{D} = \frac{-51}{-17} = 3$$

$$y = \frac{\begin{vmatrix} 3 & 7 & 2 \\ 1 & 6 & 1 \\ 2 & 2 & -2 \end{vmatrix}}{D} = \frac{-34}{-17} = 2$$

$$z = \frac{\begin{vmatrix} 3 & -2 & 7 \\ 1 & 1 & 6 \\ 2 & -1 & 2 \end{vmatrix}}{D} = \frac{-17}{-17} = 1$$

CHECK:

$$3x - 2y + 2z = 7$$

$$3(3) - 2(2) + 2(1) = 7$$

$$9 - 4 + 2 = 7$$

$$7 = 7$$

$$x + y + z = 6$$

$$3 + 2 + 1 = 6$$

$$6 = 6$$

$$2x - y - 2z = 2$$

$$2(3) - 2 - 2(1) = 2$$

$$6 - 2 - 2 = 2$$

$$2 = 2$$

#### C. SUBROUTINE "CRAMER'S RULE" CHECK

Running the values in Section B through the subroutines of the programs in Appendix A and Appendix B yielded the same results as the example.

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